

Analysis of the Cromwell, Minnesota Well 4 (593593) Aquifer Test

CONDUCTED ON MAY 24, 2017

CONFINED QUATERNARY GLACIAL-FLUVIAL SAND AQUIFER

**Analysis of the Cromwell, Minnesota Well 4 (593593) Aquifer Test
Conducted on May 24, 2017**

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Data Collection and Analysis

The constant-rate aquifer test performed at Cromwell 4 (593593) was conducted as described below. The test results are summarized in Table 1. The specifics of test location, scope, and timing are presented in Table 2, Table 3, and Table 4. Data were analyzed using standard methods cited in references. Individual analyses are presented the Figures 1-25 and are summarized in Table 5 and Table 6. Figures 26-44 include maps, comparison of manual and electronic data, and any other test documentation. Records of well construction are contained in Figures 45-54.

Description

Purpose of Test

The test of Cromwell 4 was conducted by the Minnesota Department of Health (MDH) Source Water Protection Unit as a small part of a longer-term project led by the United States Geological Survey (USGS). The overall purpose of the study is to assess the rates of groundwater recharge through low-conductivity glacial sediments at various sites in Minnesota.

Specific to Cromwell, eight observation wells were installed by the USGS in 2015. Water elevations were recorded on a one-hour interval in five of these wells for approximately one-year. The USGS had completed its data collection and was preparing to seal the observation wells. Prior to sealing the wells, notification was provided to the partner agencies relative to the completion of the work. At that time, staff in the Source Water Protection Unit recognized that this configuration of observation wells is nearly ideal for conducting a short-term constant-rate aquifer test that is designed to estimate vertical groundwater flow induced by pumping. Therefore prior to sealing the wells, MDH proposed to conduct tests that would complement the USGS data collection efforts.

Well Inventory

The well records are presented in Figures 45-54 and the well construction is summarized in Table 2. Detailed site plans are shown in Figure 26 and Figure 27.

Hydrogeologic Setting

These records were used to assess the hydrogeologic setting and identify the appropriate conceptual model for data analysis. A schematic section through the test site is shown on Figure 28 to illustrate the three layers that comprise the flow system; water table, aquitard, aquifer, and the construction of wells within these layers.

Other Interfering Wells

No other high capacity wells exist in the area to cause interference.

Test Setup

The USGS provided the pressure transducers and data loggers used for long-term monitoring, re-programmed to a one-minute interval. MDH hydrologists, Tracy Lund and Justin Blum, traveled to Cromwell on May 18, 2017 to assess site conditions and re-install the transducers to collect background water level and barometric data. At that time, the flowmeter-totalizer had been removed for cleaning and calibration. Mr. Tom Johnson, the water operator, indicated that the flowmeter would be returned to service shortly and the test was tentatively scheduled to begin on May 23, 2017.

Access to Cromwell 3 (519761) is restricted and the only means to measure the water level is via a bubbler-line. A transducer could be placed in Cromwell 4 to monitor water levels. A prior test of Cromwell 3 was conducted by the MDH in 2001. The location of the obwell nests relative to the PWS wells is slightly closer to Cromwell 4 than 3. The obwells constructed in the till are within 60 feet of Well 4 and are therefore more likely to respond to pumping. Because of these factors; access to the wells, prior tests, and the relative distance of the well nests, caused Cromwell 4 to be preferred for testing.

After the flowmeter was reinstalled, MDH staff mobilized for the test on May 24, 2017, arriving on-site at 10:00. The flow monitoring equipment and pump controls were inspected with the operator. Discussions with the operator indicated that the system demand is much smaller than the capacity of the well and water will have to be wasted during the 24-hour pumping phase. He considered putting a discharge control on one of the hydrants to drain the excess but opted to let the tower fill and overflow to the established drain. This presented no flooding or erosion hazard and did not require monitoring for concerns of public safety.

An MDH pressure transducer was installed in Cromwell 4; programmed to a 20 second interval, and scheduled to begin data collection 5/24/2017 at 12:00. Static levels were collected from all accessible wells prior to beginning the test. A transducer (in-line with a compressor) was attached to the Cromwell Well 3 bubbler-line to attempt to collect water levels.

Weather Conditions

Conditions were cool and rainy during background data collection. No appreciable precipitation occurred during pumping and recovery.

Discharge Monitoring

The totalizing flow meter was read manually to document the pumping rate. The operator flushed hydrants between 12:30 and 15:00, early in the pumping phase, putting some of the excess water to productive use.

Data Collection

The pump was started at 12:10:04 on 5/24/2017 by hand control. The compressor/transducer setup on Well 3 did not collect usable data. Water levels were collected manually from the accessible wells and data were downloaded to check the operation of the transducers.

It was found that the transducer in well USGS 2-E (773064) was set too deep in the well and did not collect usable data during background and early pumping. The submergence of the transducer was adjusted and a static collected at 15:30. Data collected after about 280

minutes of pumping (~18:00 on 5/24/2017) are valid. The transducers in all other observation wells appeared to functioning properly.

In the morning of 5/25/2017 distances from the pumped well to the observation wells and other features visible on aerial photos were measured with fiberglass tape. Data were downloaded from the transducers prior to end of pumping/start of recovery. Recovery began at 12:25:00 5/25/2017.

During the recovery period, over the Memorial Day weekend, the water operator agreed to manipulate the pump controls in such a way that Well 4 would not be pumped and Well 3 would be used to meet demand. Normal operation is to alternate the wells, accomplished by an automatic switch in the pump controls. Bypass of the switch provided data from short-term pumping of Well 3 to compare to that from the test of Well 4, just completed, see test 2613.

Data were downloaded on 5/30/2017 and water levels measured. The recovery-phase data from USGS 1-A was lost during the download process. Also, inspection of the data from Well 4 showed that the hydrant flushing caused anomalous changes in water level in the early part of the pumping-phase. Because of these problems, it was decided to perform a second, short-term constant-rate test, of Well 4 to attempt to collect additional early-time data from the pumped well and USGS 1-A. This test was run the same way as the earlier constant-rate test but for an abbreviated pumping period (345 minutes) with an overnight recovery. The final water levels were measured on 5/31/2017 and the equipment removed from the wells. Results of this short-term test are described in a separate document, see test 2619.

Qualitative Aquifer Hydraulic Response

Detailed site plans are shown in Figure 26 and Figure 27, identifying the wells and distances between the wells. A schematic cross section is provided for visual context of the test conditions, Figure 28. Comparison of manual and transducer data are shown Figure 29 through Figure 37. All but one well showed a response to pumping. USGS 2-A, constructed in the water table aquifer showed no response, as expected. The groundwater gradient is upward under 'static conditions,' including typical pumping to meet the system demand, Figure 38. The ambient difference in water elevation across the till at the well site is approximately 8.4 feet. Comparisons of water elevations between wells at the nests are shown on Figure 39 and Figure 40. From these comparisons, the more intensive pumping of this constant-rate test temporarily reversed the gradient within a short distance from the pumped well (~10 feet) and generated a strong signal for analysis of hydraulic properties.

The water elevations appear to trend upward over the data collection period. No appreciable change in water level can be attributed to changes in barometric pressure, Figure 41. The trend of the increase in water level shown on Figure 37 was removed prior to analysis.

The only truly anomalous hydraulic responses were seen in wells USGS 2-B and 2-C, Figure 34 and Figure 35, respectively. These wells showed consistent, transient, reverse water level variation with the start of pumping of either Cromwell 3 or 4; conditions under which elevations would be expected to decrease. The reverse water variation also occurred at the end of the Cromwell 4 pumping phase. The magnitude of the response was about 0.1 foot and dissipated within about twenty minutes of the change in conditions. This phenomenon has been described in the literature as a poro-elastic response, Wolf (1970). Reverse water level fluctuations are characteristic of wells constructed in materials with a low conductivity and high elasticity (clay) that are in contact with materials of high conductivity and high compressive strength (sand). This condition is rarely observed and is the first time that it has been encountered (that we are aware of) in Minnesota. Because of this poro-elastic

response, data from these wells are considered to be most representative of conditions within the till, relative to the response of other wells in this nest.

Within the aquifer itself, the simplifying assumptions of commonly used analysis techniques consider the movement of groundwater induced by pumping to be exclusively horizontal. In the case of this analysis, vertical head differences within the aquifer within 200 feet of the pumped well cannot be neglected. The pumping well is constructed with a twenty-foot screen, centered 55 feet below the top of the sand and gravel aquifer. The total thickness of the aquifer in this location is 145 feet. This type of well construction where the aquifer is screened over only a portion of the whole thickness is known as 'partially penetrating.' Because of this well construction, within small radial distances (tens of feet) from the pumped well, groundwater flow is spherical rather than horizontal; transitioning to horizontal with increasing radial distance. The rule of thumb (Hantush, 1964) for estimation of the radial distance at which this transition to horizontal flow is complete:

$$r_h = 1.5 * (\text{aquifer thickness}) * \left(\frac{\text{horizontal conductivity}}{\text{vertical conductivity}} \right)^{0.5}$$

Given the geometry of aquifer materials and well construction at this site; and, if there is no difference between horizontal and vertical hydraulic conductivity, then the minimum distance to the transition to horizontal flow is 217 feet. [In fluvial sediments, the vertical conductivity is normally smaller than the horizontal conductivity – increasing differences between these conductivities will produce a progressively larger radial distance of transition.] Both well nests are within this minimum distance and therefore the effects of partial penetration should be expected to be present.

The partially penetrating condition was verified in Aqtesolv, Figure 42, as being the result of spherical flow by the similarity of the slope of data to the diagnostic curve. A non-Theisian response was also seen by the approximate unit-slope of early-time data USGS 1-B, on a log-log plot before 200 minutes, Figure 43. The portion of the transient response before 200 minutes, dominated by spherical flow, should not be used for analysis by methods that do not incorporate partial-penetration.

An additional consideration for the analysis of aquifer properties is the decrease in conductivity at the top of a layer resulting from fluvial depositional processes. This is typically described as the 'fining upward' distribution of grain-size when looking at layers of sediment in cross-section. Because of this tendency, it is expected that the conductivity of the material at the top of the aquifer would be smaller than that at the level of the pumped-well screen or at the base of the aquifer.

This expectation is consistent with the remarkable similarity of the observed hydraulic response of USGS 1-B and 1-C, in the middle and at the base of the aquifer, Figure 43 and Figure 44. The similarity of response indicates a negligible contrast in horizontal and vertical conductivities for middle to lower parts of the aquifer. With regard to the response at the top of the aquifer, a smaller conductivity normally implies a larger drawdown. However, the drawdown at the top of the aquifer cannot be greater than that observed at USGS 1-B, at the level of the pumped-well screen within the aquifer. This represents a bounding condition on estimates of drawdown, useful to inform the analysis.

Quantitative Analysis

Typically, an aquifer test characterizes the hydraulic properties of aquifer materials and if additional information can be extracted relative to the bounding aquitards; it is generally considered a 'bonus.' However, the primary question for this project is the assessment of

the vertical movement of water in the till. Therefore, the goals of this project require a different approach.

The difference in water pressure across the aquitard drives the leakage through the till. The pressure at the top of the aquitard is well documented (USGS 2-A); but, is unknown at the base of the aquitard/top of aquifer. The uncertainty is the result of the effects of the partially-penetrating pumping well. Consequently, uncertainty in the drawdown at the boundary between the aquifer and till causes uncertainty in the leakage rate. Because of these complications, the analysis must proceed in stages and must be checked at each stage for consistency with the conceptual model of a partially penetrating well in a leaky-layered system.

The analysis process is broken into parts or steps that use different groups of wells to focus on how the aquifer works (conceptual models). Steps 1 through 4 lead to an assessment of representative (bulk) properties of the aquifer and aquitard. Step 5 is the analysis by the Neuman-Witherspoon method that emphasizes the impact of lithological variation within the till on hydraulic response and estimated aquifer properties. These different views of the data and how the aquifer works must converge to a set of relatively consistent aquifer properties for there to be some confidence in the test results.

Transient-Horizontal Flow

The hydraulics of a partially-penetrating pumping well has been developed in the literature with several published solutions. Some of these solutions have been implemented in the commercial aquifer test analysis software, Aqtesolv, (Duffield, 2007). This tool was used to simulate the aquifer response by a method that includes partial-penetration and leakage, a solution referenced to Hantush-Jacob (1955).

The base data set for the simulation included data from the pumped well and USGS 1-B. The goal of these simulations was to solve for reasonable aquifer properties and predict the drawdowns at the nest locations at the base of the till/top of the aquifer. The drawdown was simulated as 'virtual piezometers' at these locations. The solutions from these analyses uniformly produced very large transmissivity, small storativity, and large leakage factor, Figure 1. Well USGS 1-C was included in the solution shown on Figure 2. These simulations were not judged to be realistic because drawdowns at the virtual piezometers were uniformly smaller than that predicted by the response of the USGS obwells. It was found that inclusion of data from the pumped well was forcing an inappropriate solution.

The analysis based on data from only USGS 1-B is considered to be most reasonable to begin this process, Figure 3. This analysis produced aquifer properties that are in the reasonable range for transmissivity and storativity; including a vertical/horizontal conductivity ratio of ~ 0.5 and a leakage factor of ~ 360 feet ($1/B = 2.8e-3$). As the focus of this analysis is the properties of the till, the conductivity ratio and leakage factor are useful to simulate the effects of pumping at the base of the till at Nests 1 and 2. The transmissivity at the base of the till is expected to be in the range of $2,200 \text{ ft}^2/\text{day}$. And, based on this leakage factor, the X-axis intercept (semi-log plot of distance drawdown) is expected to be in the range of 400 feet ($L * 1.12$). Based on the aquifer properties from Figure 3, the drawdowns at the virtual piezometers are modeled to be in the range of 5 and 3 feet at Nests 2 and 1, respectively.

Steady-State Horizontal Flow

A distance-drawdown plot is used for the combined transient (Cooper-Jacob [1946]) and steady-state analysis (Hantush-Jacob [1955]), Figure 1 through Figure 4. This view of the aquifer response, based only on Cromwell 4 and USGS 1-B, produces a large transmissivity

and large leakage factor (very low rate of leakage). The quantities are incorrect because the conceptual model is incomplete (no partial-penetration or anisotropy). The utility of this plot is that the slope of this regression defines the maximum drawdown in the aquifer system at any radial distance. Therefore, the estimated drawdown at Nest 2 cannot be greater than ~5.3 feet.

Steady-State Vertical Flow

At Cromwell, the till is quite leaky and all observation wells constructed within the till clearly responded to pumping. The number of observation wells at Nest 2 provides the most direct estimate of water pressure at the base of the till/top of the aquifer. The configuration of the well nest is analogous to test column of granular material in the laboratory where observation wells act as individual pitot tubes.

A linear regression of the observed drawdowns from the Nest 2 observation wells, after 1450 minutes of pumping and projected to 10,000 minutes, Figure 5. These values were used to estimate the possible drawdown at the base of the till, ranging from 4.8 to 5.8 feet, Figure 6. Lithological differences between USGS 2-D and USGS 2-E are the cause for this large range. The regressions that followed the trend of wells USGS 2-B and 2-C were favored because of reasons discussed above. Additionally, there are physical limits on the drawdown at the base of the till, as discussed above. The range of drawdown at Nest 2 from this analysis is consistent with that from the steady-state horizontal flow of approximately 5.3 feet.

The drawdown at Nest 1 can only be roughly estimated because a single observation well was constructed in the till, USGS 1-A. A similar regression to that described above was performed to estimate the drawdown at the base of the till at this Nest. Figure 7 shows these regressions at, 2.0 and 2.95 feet at 1450 minutes and 10,000 minutes, respectively. This is also consistent with the constraints on drawdown from Figure 4.

Steady-State Leakage Caused by Pumping

The consistency of these estimates was checked on a semi-log plot of distance-drawdown by comparing the slopes and X-axis intercepts, Figure 8 and Figure 9. These possible solutions produce a similar point of zero drawdown at 400 to 500 feet and reasonable transmissivities for aquifer materials at the base of the till. The storativity from these solutions is not valid because of the effects of partial penetration; however, these large values for storativity are reasonable with respect to the time that it takes for the response to pumping to propagate to the base of the till.

The leakage factor is essential for calculating the vertical conductivity of the till in combination with other parameters: transmissivity and aquitard thickness. Here, the notation for leakage factor, 'L' from Kruseman and de Ridder (1991) is used. The leakage factor from the steady-state Hantush-Jacob analysis is calculated as, $L = X_0 / 1.12$. The equation for the vertical hydraulic resistance of the aquitard is, $c = L^2/T$ in units of days.

From these relationships, the vertical conductivity is calculated (in terms of L) as,

$$k_v = b' / (L)^2 / T]$$

As shown in Figure 9, the Hantush-Jacob analysis of distance-drawdown data produces,

$$k_v = 130 / [(437)^2 * 2200] = 1.5 \text{ ft/day.}$$

Simultaneous Solution for Horizontal and Vertical Flow

The transient response of the observation wells constructed within the till can be analyzed by the Neuman-Witherspoon method. The responses at Nests 1 and 2 were analyzed separately and as a composite, Figure 11 through Figure 21.

The Nest 2 analyses, generally were consistent values for aquifer properties. The analysis of recovery data at Nest 2, Figure 17, produced the best match and results that most closely followed the analysis of USGS 1-B, Figure 3.

The Neuman-Witherspoon analyses from Nest 1, Figure 18 and Figure 19, produced a larger transmissivity and a larger vertical conductivity of the till. Figure 18 attempted to match the data from within the aquifer. The solution shown on Figure 19 was based on the single till observation well, USGS 1-A.

The composite analyses, matching all data from the obwells were lower quality matches and more variable results, Figure 20 and Figure 21.

Estimates of leakage factor from factor from the Neuman-Witherspoon analyses are reported as $1/B$. This parameter is the same as the 'B' in 'r/B' from the steady-state Hantush-Jacob model, Walton (1960) normalized for radial distance. $1/B$, is the inverse quantity, $L = (1/B)^{-1}$, and the vertical hydraulic resistance is expressed as, $1/c = (1/B)^2 * T$ in units of days⁻¹.

From these relationships, the vertical conductivity is calculated (in terms of $1/B$) as,

$$k_v = b' * [(1/B)^2 * T]$$

As shown in Figure 17, the Neuman-Witherspoon analysis of data from Nest 2 produces,

$$k_v = 130 * [(0.0017)^2 * 2300] = 0.86 \text{ ft/day.}$$

Heterogeneity in the properties of the till is indicated by the poor match of the response of USGS 1-E to the curves relative to the other wells in Nest 2, Figure 17. Examination of the slopes of the late-time data at the observation wells in the till shows that there is a marked similarity in the trends of USGS 1-A and USGS 2-E, Figure 22. Because of this similarity a separate Neuman-Witherspoon analysis was performed on only those wells, Figure 23. This analysis is a reasonable upper bound on the conductivity of the till, 4.1 ft/day.

Additional Analyses for Comparison to other Parts of the Dataset

Figure 24 and Figure 25 are recovery analyses for comparison to the short-term tests that were conducted after this test, see documents for tests 2613 and 2619.

Conclusion

The bulk aquifer and aquitard properties from this dataset are shown in Table 1, as derived from the analyses listed on Table 5 and Table 6. This test is a detailed examination of the properties of the till in a very small area. The large range of estimated aquifer properties result from both: the sub-set of the data to which an analysis method was applied, and natural lithological variation, particularly within the till.

The reported range of vertical conductivity of the till is from 0.85 to 4.1 ft/day. The low value, 0.85 ft/day, is from the response of wells at Nest 2, USGS 1-B, 1-C and 1-D.

However, the till contains significant heterogeneities and the vertical conductivity is significantly greater in some areas. Based on the responses at USGS 1-A and USGS 2-E, the largest credible value from this dataset is 4.1 ft/day. Because these wells are at both nests, it is likely that this analysis characterizes the till over a larger geographic extent than the analyses from the observation wells limited to Nest 2. Therefore, for modelling purposes it is unlikely that the low value is realistic and a more reasonable range of the bulk properties of the till is from 1.1 to 4.1 ft/day.

Acknowledgements

There have been few opportunities to collect this level of detailed hydraulic information for the analysis of rates of leakage through till. It is judged that this data collection effort and subsequent analysis was particularly successful, given the hydrogeologic setting and the normal challenges of adapting to field conditions. Credit for this success is due in large part to the active participation and support of Mr. Tom Johnson, water operator for the city of Cromwell. Thank you.

References

- Agarwal, R.G. 1980. A new method to account for producing time effects when drawdown type curves are used to analyze pressure buildup and other test data. SPE Paper 9289, presented at the 55th SPE Annual Technical Conference and Exhibition, Dallas, Texas, September 21–24, 1980.
- Blum, J. L. (2017a) Analysis of Four Short-term Pumping Tests Conducted at Cromwell 3 (519761), May 26 - May 30, 2017, Confined Quaternary Glacial-Fluvial Sand Aquifer. Technical Memorandum - Aquifer Test 2613. Minnesota Dept. of Health, pp. 34.
- Blum, J. L. (2017b) Analysis of Short-term Pumping Test of Cromwell 4 (593593), May 30, 2017, Confined Quaternary Glacial-Fluvial Sand Aquifer. Technical Memorandum - Aquifer Test 2619. Minnesota Dept. of Health, pp. 22.
- Cooper, H.H. and Jacob, C.E. (1946) A Generalized Graphical Method for Evaluating Formation Constants and Summarizing Wellfield History, *Trans. American Geophysical Union*, V. 27, pp. 526 – 534.
- Kruseman and De Ridder, (1991) *Analysis and Evaluation of Pumping Test Data* (2nd Edition), Publication 47, International Institute for Land Reclamation and Improvement, P.O. Box 45, 6700 AA Wageningen, The Netherlands, pp. 76-78.
- Duffield, G.M. (2007) *AQTESOLV for Windows Version 4.5 User's Guide*, HydroSOLVE, Inc., Reston, VA.
- Jacob, C.E. (1947) Drawdown Test to Determine the Effective Radius of Artesian Wells. *Transactions of the American Society of Civil Engineers*, 112, pp.1047–1170.
- Hantush, M. (1964) 'Hydraulics of Wells', in Chow, V. T. (ed.) *Advances in Hydroscience*. New York: Academic Press. Available at: <http://www.ees.nmt.edu/hantush/213-hantush-wellshydrolics>.
- Hantush, M. S. and Jacob, C.E. (1955a) Non-steady Radial Flow in an Infinite Leaky Aquifer, *Trans. American Geophysical Union*, Vol. 35, pp. 95-100.

- Hantush, M. S. and Jacob, C.E. (1955b) Steady Three-dimensional Flow to a Well in a Two-layered Aquifer, *Trans. American Geophysical Union*, Vol. 36, pp. 286-292.
- Lund, T. and Blum, J.L. (2017) Analysis of the Cromwell 4 (593593) Pumping Test, May 24, 2017, Confined Quaternary Glacial-Fluvial Sand Aquifer. Technical Memorandum - Aquifer Test 2612, Minnesota Dept. of Health, pp. 70.
- Neuman, S.P. and Witherspoon, P.A. (1969) Theory of flow in a confined two aquifer system, *Water Resources Research*, vol. 5, no. 4, pp. 803-816.
- Theis, C. V. (1935) The Relation Between the Lowering of the Piezometric Surface and the Rate and Duration of Discharge of a Well Using Ground-Water Storage, *Trans. American Geophysical Union*, 16th Annual Meeting, April, 1935, pp. 519-24.
- Walton, W.C. (1960) Leaky Artesian Aquifer Conditions In Illinois, *Illinois State Water Survey, Bulletin 39*, pp. 27.
- Wolff, R. G. (1970) Relationship between horizontal strain near a well and reverse water level fluctuation, *Water Resources Research*, 6(6), pp. 1721-1728.

Tables and Figures

Table 1. Summary of Results for Leaky Confined - Radial Porous Media Flow

Parameter	Value	Unit	Range Minimum	Range Maximum	+/- % variation
Top Stratigraphic Elev.	1152	feet (MSL)			
Bottom Stratigraphic Elev.	1007	feet (MSL)			
Transmissivity (T)	4,400	ft ² /day	1,000	5,700	
Aquifer Thickness (b)	145	feet	145	175	
Hydraulic Conductivity (k)	30	ft/day			
Ratio Vertical/Horizontal k ¹	0.5	0.00 %			
Primary Porosity (e _p)	0.25	0.00 %			
Storativity (S)	2.0e-4	dimensionless	1.0e-4	4.0e-4	
Characteristic Leakage (L)	500	feet	330	2610	
Hydraulic Resistance (c)	114	days	50	220	
Thickness of till (b')	130	feet			
Hydraulic Conductivity of till (k _v)	1.1	ft/day	0.8	4.1	

¹ Conductivity decreases to ~15 ft/day at top of aquifer (transmissivity, ~2,200 ft²/day)

Table 2. Aquifer Test Information

Information Type	Information Recorded
Aquifer Test Number	2612
Test Location	Cromwell 4 (593593)
Well Owner	City of Cromwell
Test Conducted By	MDH - T. Lund and J. Blum
Aquifer	QBAA
Confined / Unconfined	Confined
Date/Time Monitoring Start	05/18/2017 11:40
Date/Time Pump off Before Test	5/23/2017 4:31
Date/Time Pumping Start	5/24/2017 12:10:04
Date/Time Recovery Start	5/25/2017 12:25:00
Date/Time Test Finish	5/31/2017 11:00
Pumping time (minutes)	1454.93
Totalizer – end reading	106059750
Totalizer – start reading	105817400
Total volume (gallons)	242350 gallons
Nominal Flow Rate	167 (gallons per minute)
Number of Observation Wells	8 (see Table 3)

Table 3. Well Information

Well Name (Unique Number)	Easting Location, X ² (meter)	Northing Location, Y ² (meter)	Radial Distance (feet)	Ground Surface Elevation, GSE ³ (feet, MSL)	Measuring Point Description GSE+(stick-up) (feet, MSL)	Open Interval Top (feet, MSL)	Open Interval Bottom (feet, MSL)	Aquifer
Cromwell 4 (593593)	28.9	44.2	0.4	1328	~1329	1118	1098	QBAA
Cromwell 3 (519761)	62.5	45.3	112 ⁴	1328	~1330	1148	1138	QBAA
Nest 1								Till - QBAA - Bedrock
USGS C1-A (773071)	50.0	6.4	149.5	1326.3	1328.66+	1181.7	1178.9	Till – mid
USGS C1-B (773070)	48.8	6.3	147.8	1326.3	1328.62+	1105.4	1095.8	QBAA
USGS C1-C (773069)	47.3	6.4	145.6	1326.2	1328.78+	996.7	987.1	Thompson Fm.
Nest 2								Till - QWTA
USGS C2-A (773068)	40.6	54.0	53.9	1332.3	1334.67+	1300.0	1297.3	QWTA
USGS C2-B (773067)	40.6	56.1	58.8	1332.6	1334.98+	1275.9	1273.2	Till - top
USGS C2-C (773066)	42.2	54.0	57.7	1332.3	1334.71+	1253.6	1250.9	Till – mid top
USGS C2-D (773065)	39.1	54.0	50.9	1332.1	1334.58+	1228.5	1225.9	Till – mid
USGS C2-E (773064)	39.0	56.1	56.0	1332.4	1334.81+	1206.6	1204.0	Till - deep

² Local Datum³ Vertical Datum: NAV88⁴ Distance between well center, distance between outside of casing is 111 ft.

Table 4. Data Collection⁵

Data File Name: Well Name_Unique Number	Data Logger Type, SN:	Probe Id., Range (psi)	Install 1. Static WL ⁶	Install 2. XD ⁷ Setting	Remove 3. Static WL	Remove 4. XD Setting	Diff. Static WL (1-3)	Diff. XD Setting (4-2)
Cromwell- 4_593593	Troll 500 145815	17, 30 psi	15.86	12.55	15.39	13.30	0.47	0.75
Baro_data	Hermit 3000 45333	6, 15 psia						
1-A(773071)	OTT 382933		20.49	19.89	20.11	19.53	0.38	0.36
1-B(773070)	OTT 382932		16.12	15.34	15.31	14.60	0.81	0.74
1-C(773069)	OTT 382934		16.20	15.58	15.42	14.79	0.78	0.79
2-A(773068)	OTT 382929		29.69	29.04	29.48	28.70	0.21	0.34
2-B(773067)	OTT 382935		28.78	28.14	28.46	27.79	0.32	0.35
2-C(773066)	OTT 382936		26.95	26.46	26.52	26.07	0.43	0.39
2-D(773065)	OTT 382931		23.71	22.47	23.18	22.42	0.53	0.05
2-E(773064)	OTT 382937		25.15	37.16	23.65	35.60	1.5	1.56

⁵ Notes about data collection: USGS transducers/loggers installed 5/18/2017, before 12:00 on 1-minute interval. Barometer recording from 5/18/2017 11:40 on 10-minute interval. Inspected C-3 setup for logging, no access to well except by existing bubbler line. C-4 access through submersible cap, transducer installed 5/24/2017. Initial setting of transducer in USGS 2-E (773064) too deep, device did not record usable data of background and early pumping. Transducer reset on 5/24/2017 15:28. Data not recovered from USGS 1-A logger during late pumping and recovery.

⁶ WL = water level below measuring point, feet.

⁷ XD = pressure transducer depth below water surface, feet.

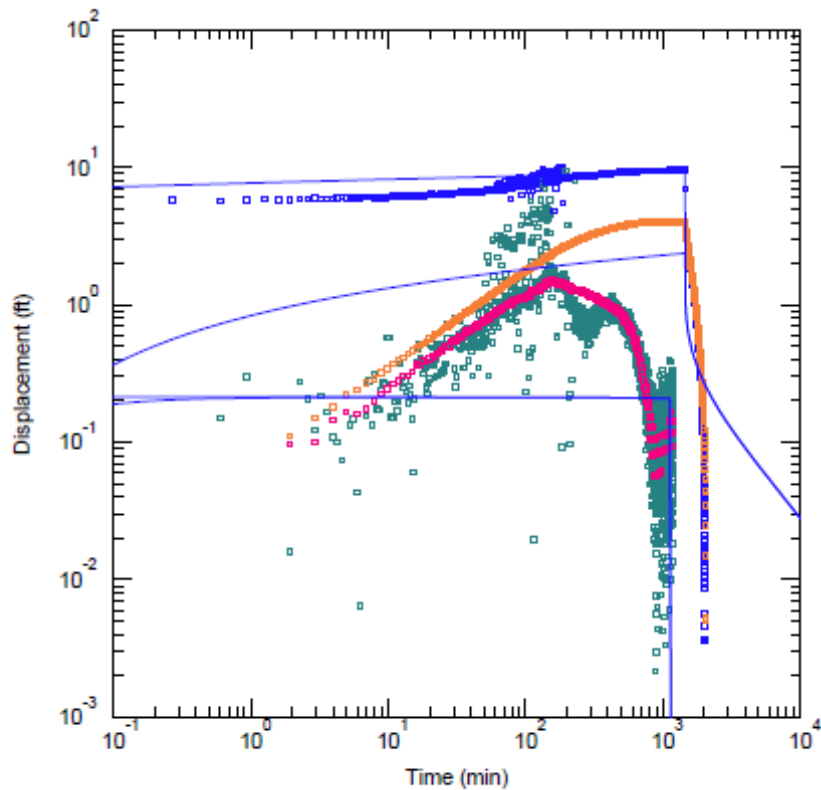
Table 5. Transient Analysis Results

Well Name (Unique Well No.)	Transmissivity, T (ft ² /day)	Storativity, S (dimensionless)	Leakage Factor, L (feet)	Hydraulic Conductivity of Aquitard, kV (ft/day)	Analysis Method	Plot No. Remarks
C-4 (593593) 1-B (773070)	12,000	2.0e-5	150,000	7.0e-5	Hantush-Jacob	1. properties not credible for very leaky system
C-4 (593593) 1-B (773070) 1-C (773069)	17,000	3.5e-4	3,570	0.17	Hantush-Jacob	2. properties not credible for very leaky system
1-B (773070)	4,380	7.7e-3	330	2.6	Hantush-Jacob	3. kz/kr = 0.5, credible properties
C-4 (593593) 1-B (773070)	5,190	1.7e-4			Cooper-Jacob	4. properties not credible for very leaky system
Nest 2, all till obwell composite	2,200	5.0e-4	590	0.83	Neuman- Witherspoon	11. credible properties, consistent with plot 9, good match
2-B (770067)	2,300	3.0e-4	500	1.2	Neuman- Witherspoon	13.
2-C (770066)	2,300	5.0e-4	500	1.2	Neuman- Witherspoon	13.
2-D (770065)	1,800	1.9e-4	380	1.6	Neuman- Witherspoon	14.
2-E (770064)	2,300	5.0e-4	500	1.2	Neuman- Witherspoon	15.
Nest 2, till obwell composite, 2-D (770065) excluded from match	2700	3.0e-3	670	0.79	Neuman- Witherspoon	16.
Nest 2, till obwell composite recovery	2,300	4.0e-4	590	0.86	Neuman- Witherspoon	17. best match
C-4 (593593) 1-B (773070) 1-A (770071)	3,730	8.0e-4	1520	2.1	Neuman- Witherspoon	18.
1-A (770071)	3,550	1.2e-3	1960	1.2	Neuman- Witherspoon	19.
All till obwell composite	1,200	2.6e-3	145	7.4	Neuman- Witherspoon	20. properties not credible, too leaky
All well composite	2,790	2.9e-3	370	2.7	Neuman- Witherspoon	21.
1-A (770071) and 2-E (770064)	1590	5.0e-2	224	4.1	Neuman- Witherspoon	23. large credible kv

Table 6. Steady-state Analysis Results

Transmissivity, T (ft ² /day)	Leakage Factor, L (feet)	Hydraulic Resistance, c (days)	Hydraulic Conductivity of Aquitard, k _v (ft/day)	Analysis Method	Plot No. Remarks
5,190	7,470	10,800	0.012	Hantush- Jacob	4. properties not credible for very leaky system
2,200	370	61	2.1	Hantush- Jacob	9. credible properties, consistent with plot 3
2,200	440	88	1.5	Hantush- Jacob	10. credible properties, consistent with plots 3 and 9

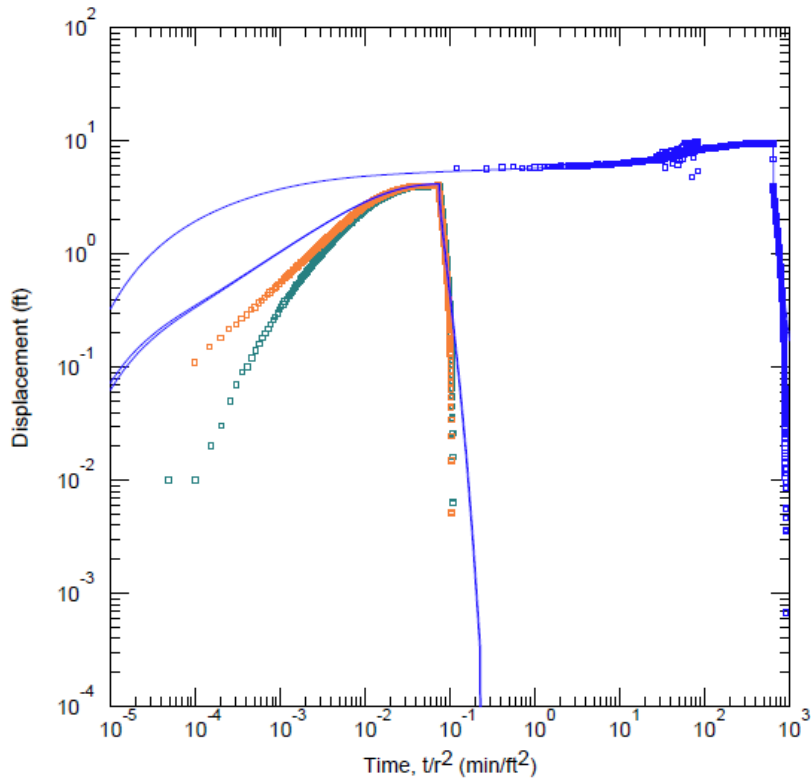
Figure 1. Solution of Aquifer Properties by Aqtesolv. Data from Cromwell 4 (593593) and USGS 1-B (773070)



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...100_Cromwell4.aqt			Time: 12:30:13		
Date: 08/22/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	□ Cromwell 4	0	0
			□ 1-B	140.5	0
			□ 1-C	140.4	0
			□ 2-B	0	54.8
			□ 2-C	0	53.2
			□ 2-D	0	46
			□ 2-E	0	51.7
<u>SOLUTION</u>					
Aquifer Model: <u>Leaky</u>			Solution Method: <u>Hantush-Jacob</u>		
T = 1.204E+4 ft ² /day			S = 1.974E-5		
1/B = 6.667E-6 ft ⁻¹			Kz/Kr = 1.		
b = 145. ft					

$L = 149,000 \text{ feet}$
 $kv = 130 * (6.7e-6)^2 * 12,000 = 7.0e-5 \text{ ft/day}$

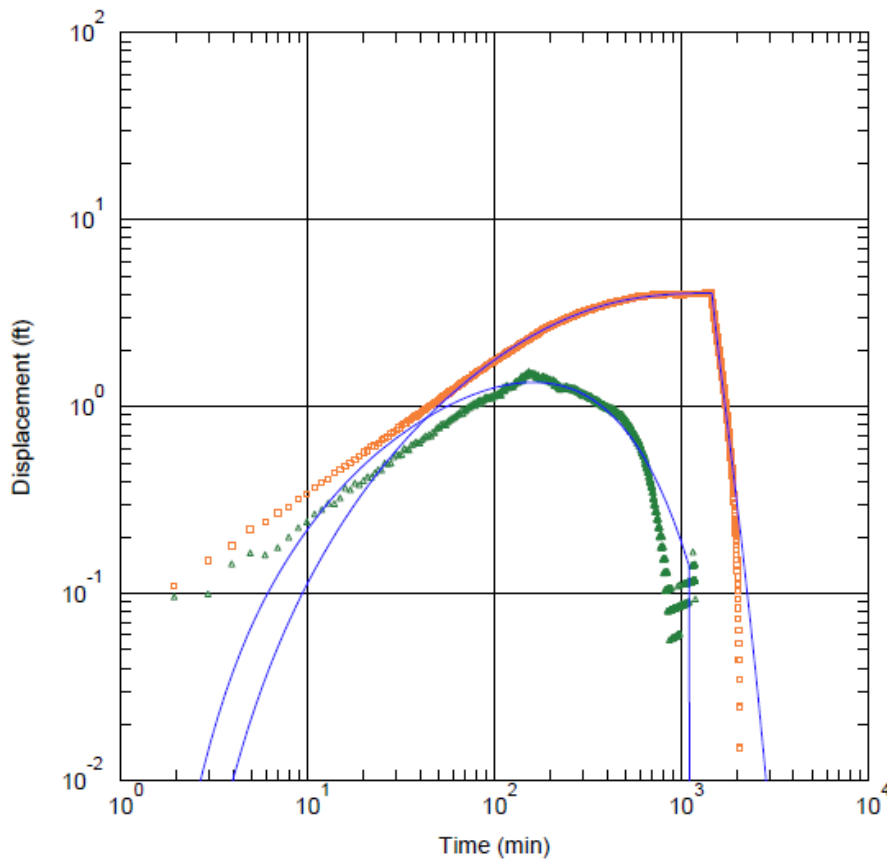
Figure 2. Solution of Aquifer Properties by Aqtesolv. Showing Data from Cromwell 4 (593593), USGS 1-B (773070) and USGS 1-C (773071)



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...00 Cromwell4_nest-1_composite.aqt			Time: 12:36:55		
Date: 08/22/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	□ Cromwell 4	0	0
			□ 1-C	139	0
			□ 1-B	140.5	0
			□ 1-A	142	0
<u>SOLUTION</u>					
Aquifer Model: <u>Leaky</u>			Solution Method: <u>Hantush-Jacob</u>		
T = 1.695E+4 ft ² /day			S = 0.0003542		
1/B = 0.0002804 ft ⁻¹			Kz/Kr = 0.5		
b = 145. ft					

L = 10,800 feet
 $kv = 130 * (2.8e-4)^2 * 17,000 = 0.17 \text{ ft/day}$

Figure 3. Solution of Aquifer Properties by Aqtesolv. Data from USGS 1-B (773070) only



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...01_cromwell_nest-1-B_partial.aqt			Time: 12:33:33		
Date: 08/22/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	1-B	140.5	0
<u>SOLUTION</u>					
Aquifer Model: <u>Leaky</u>			Solution Method: <u>Hantush-Jacob</u>		
T	= 4382.2 ft ² /day		S	= 0.007766	
r/B	= 0.4231		Kz/Kr	= 0.5	
b	= 145. ft				

L = 333 Feet
 $k_v = 130 * (0.423/141)^2 * (4380 * 0.5) = 2.6 \text{ ft/day}$

Figure 4. Conventional Distance-drawdown Plot based on Cromwell 4 (593593) and USGS 1-B (773070)

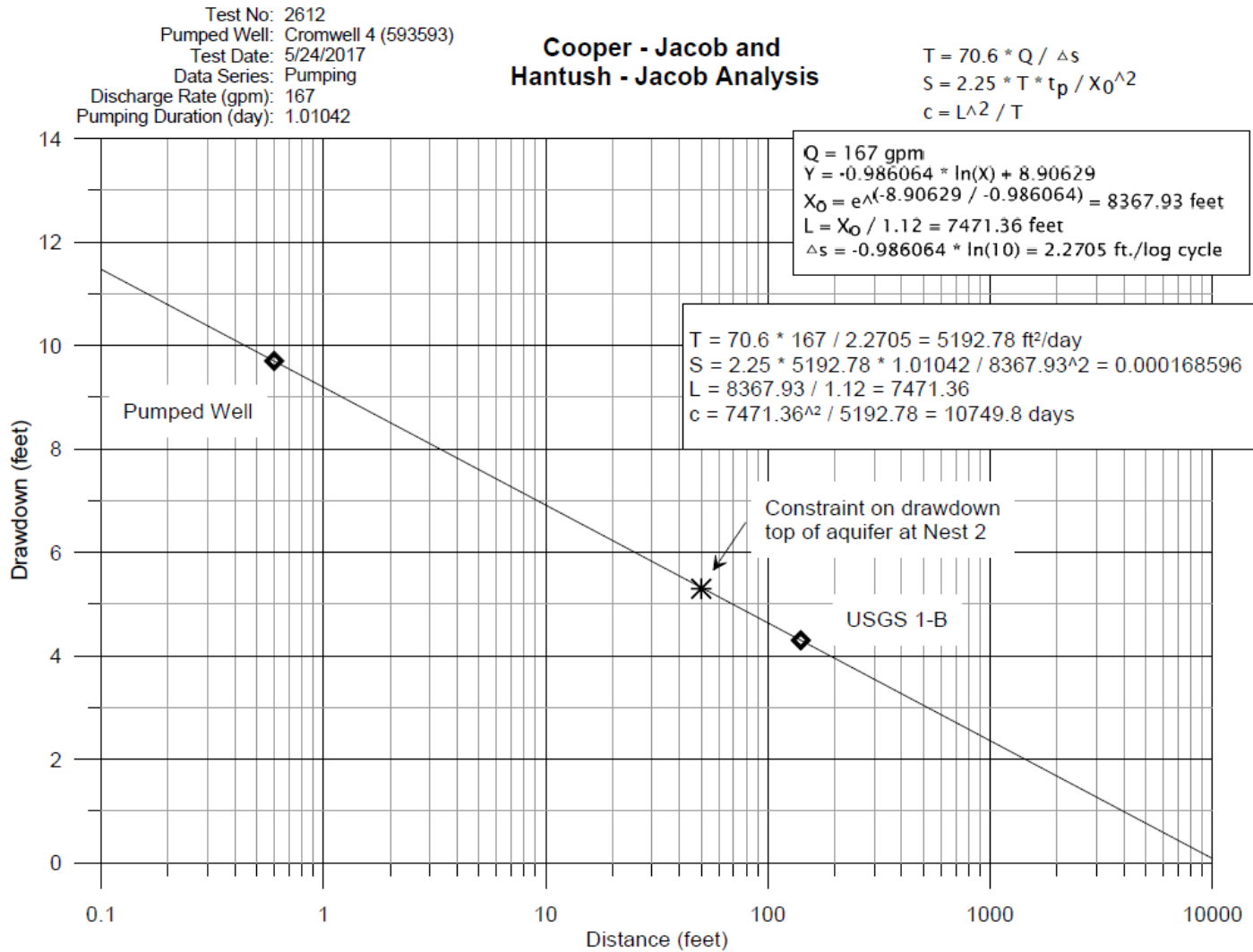


Figure 5. Drawdown at Nest 2 after 1450 minutes of pumping, projected to 10,000 minutes

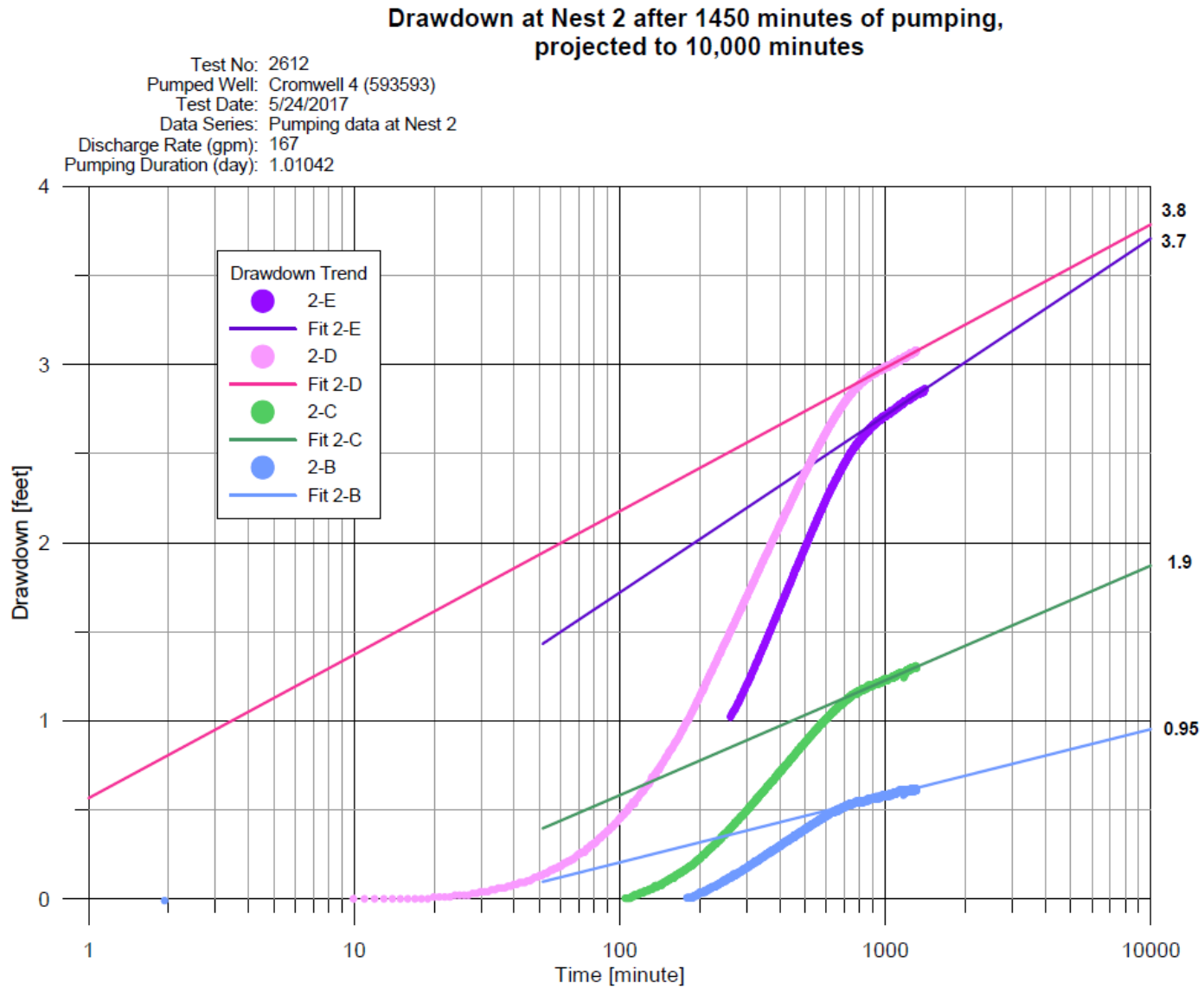


Figure 6. Groundwater Gradient at Nest 2 after 1450 Minutes of Pumping

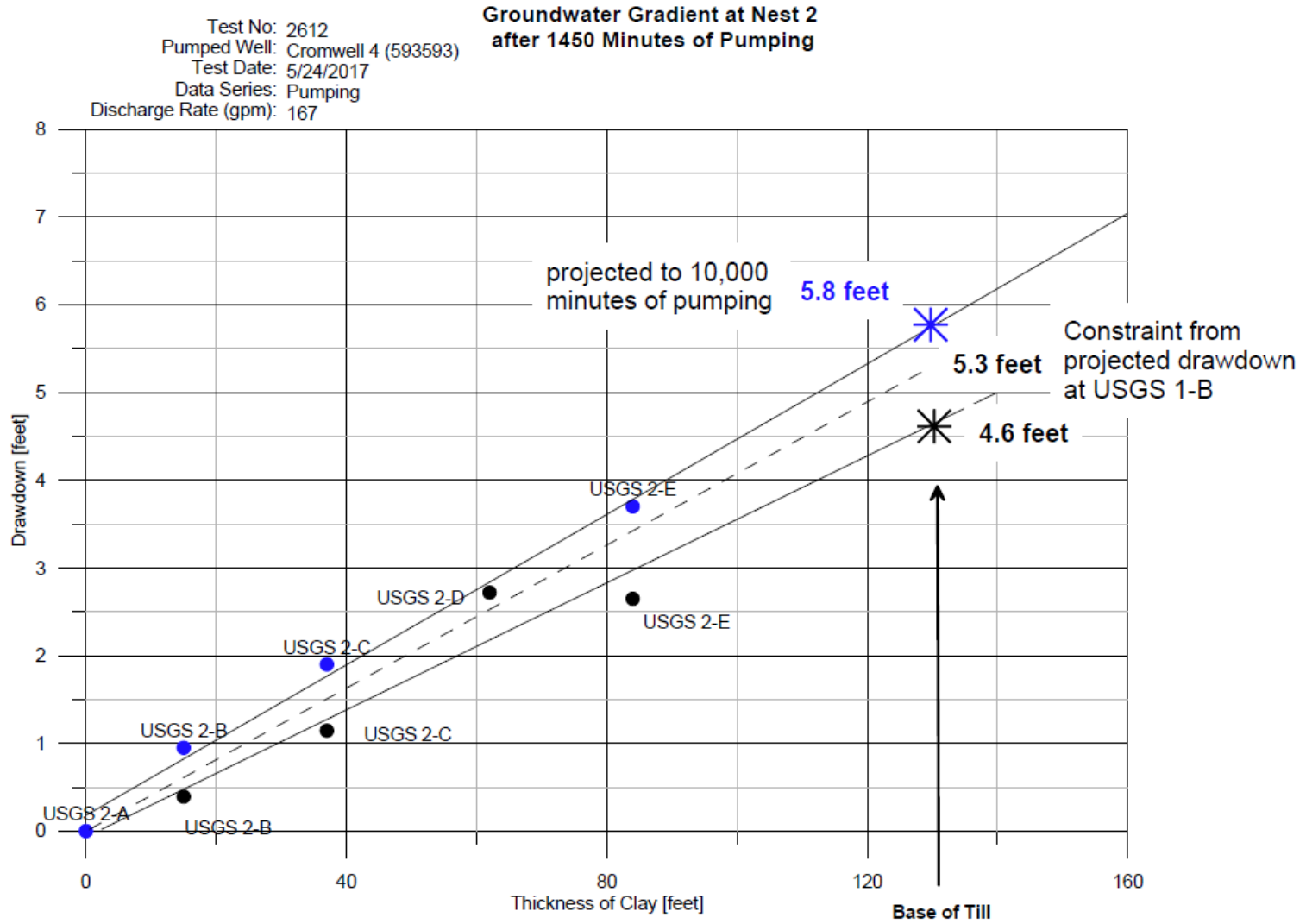


Figure 7. Drawdown at Nest 1 after 1450 minutes of pumping, projected to 10,000 minutes

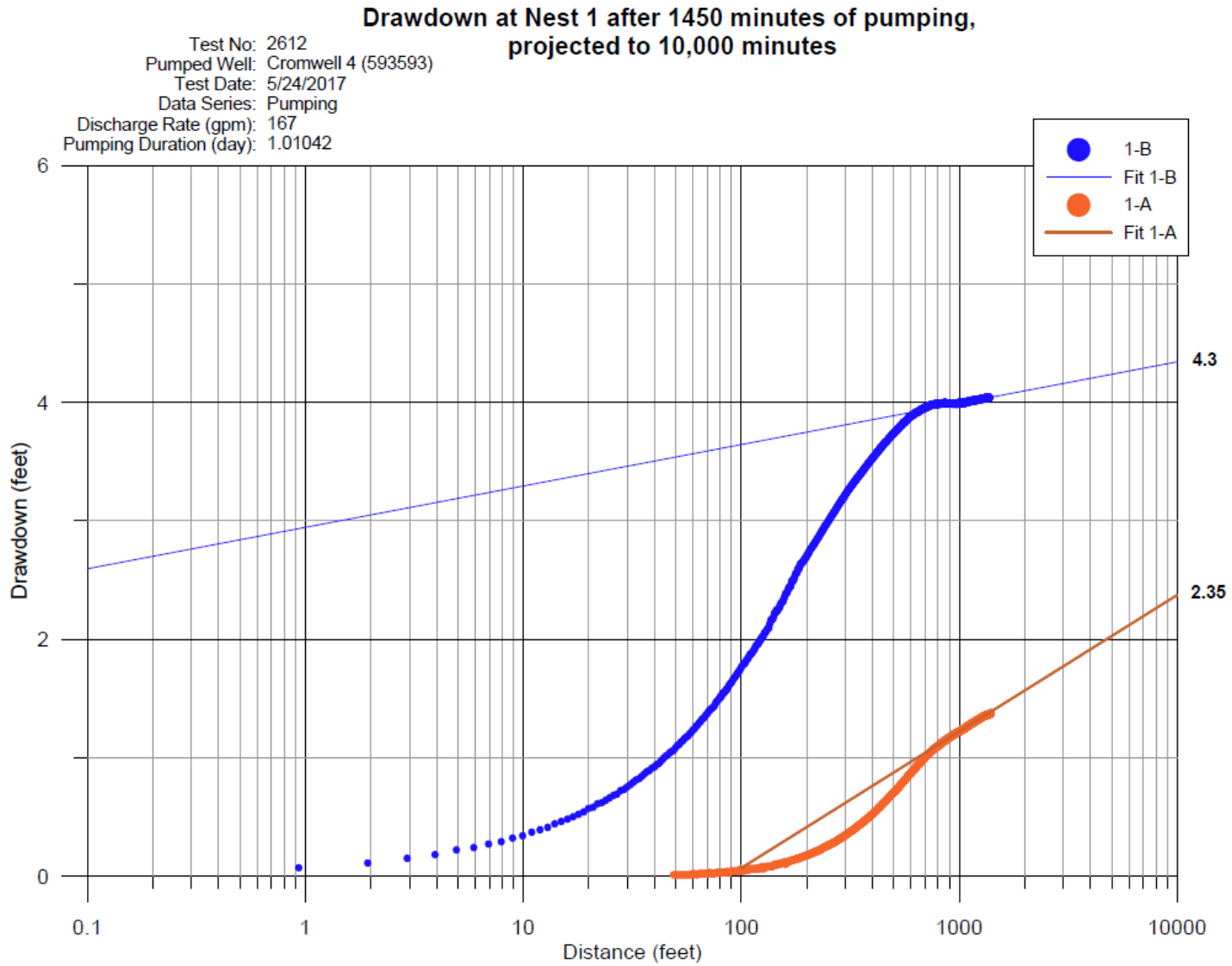


Figure 8. Groundwater Gradient at Nest 1 after 1450 Minutes of Pumping

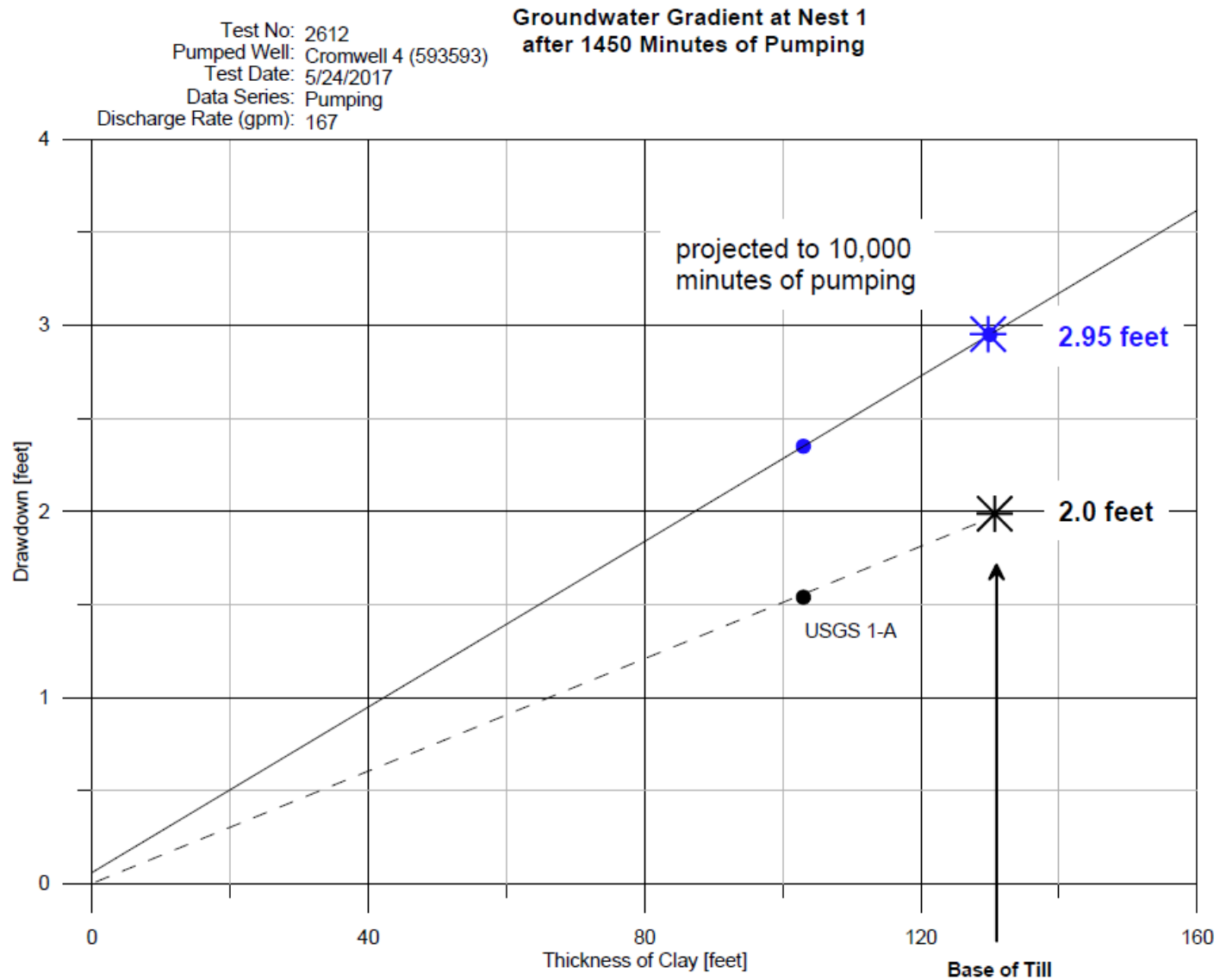


Figure 9. Comparison of Drawdowns at 1450 Minutes of Pumping at Nests 1 and 2, at Nase of Till, to that in Aquifer

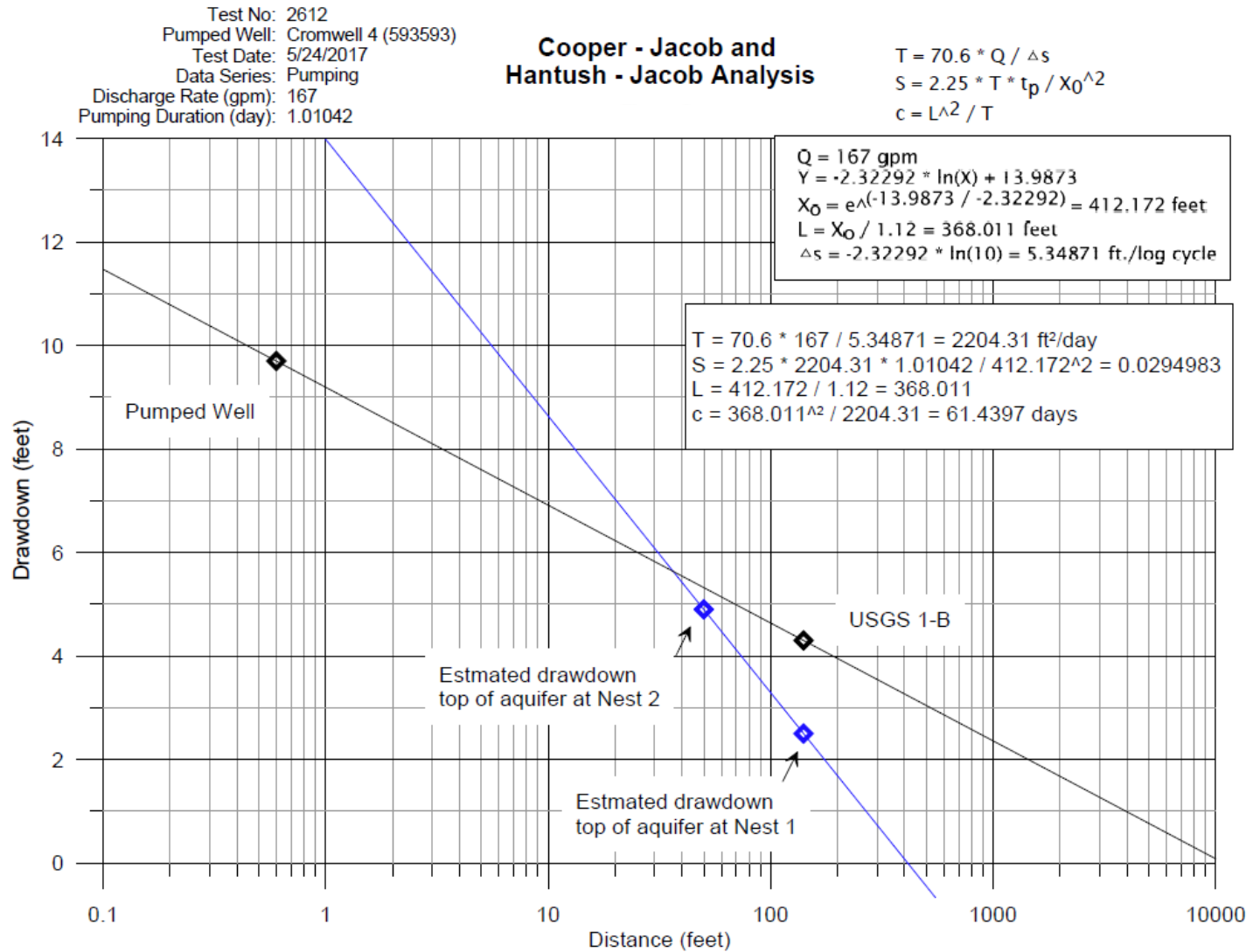


Figure 10. Comparison of Drawdowns at 10,000 Minutes of Pumping at Nests 1 and 2, at Base of Till, to that in Aquifer

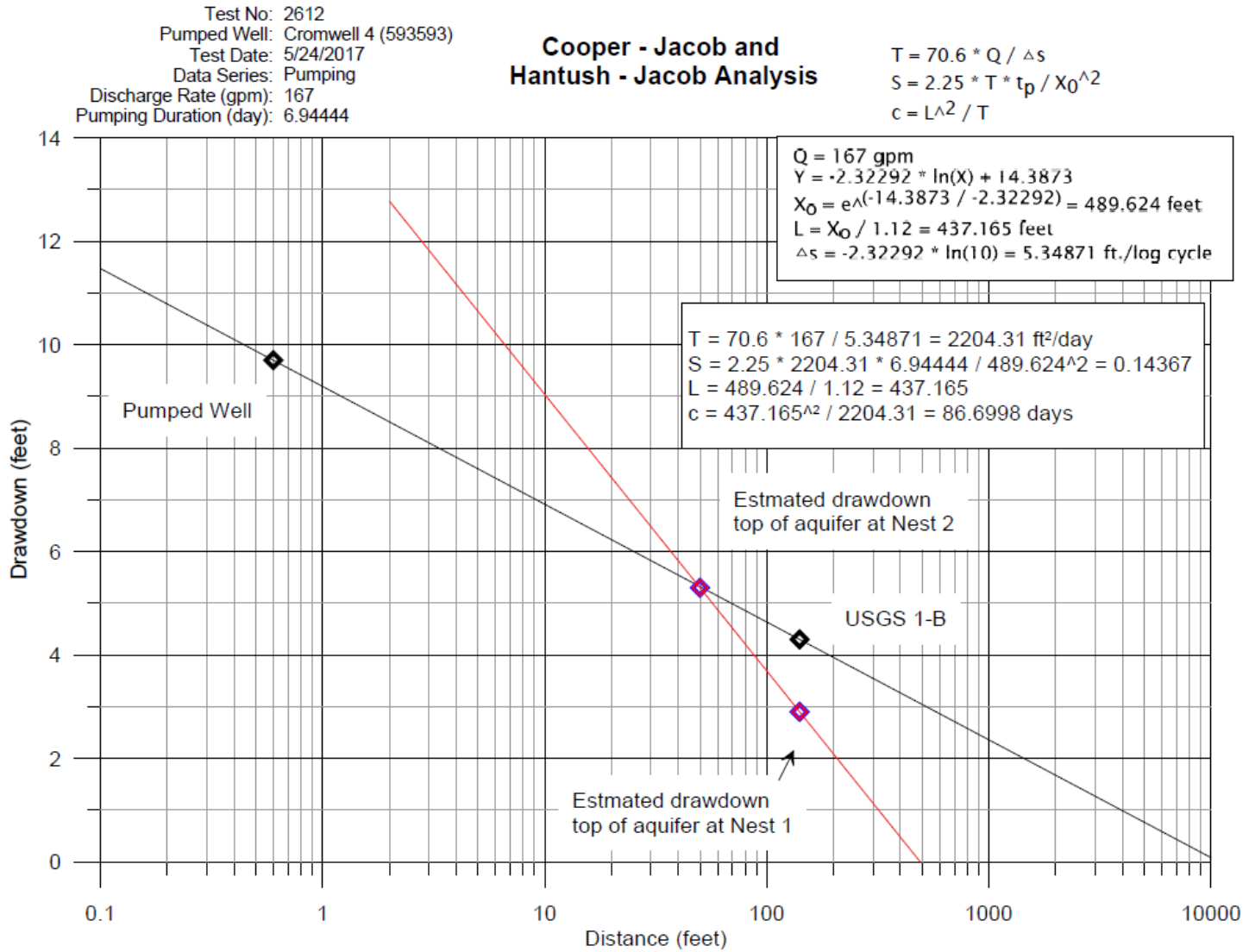
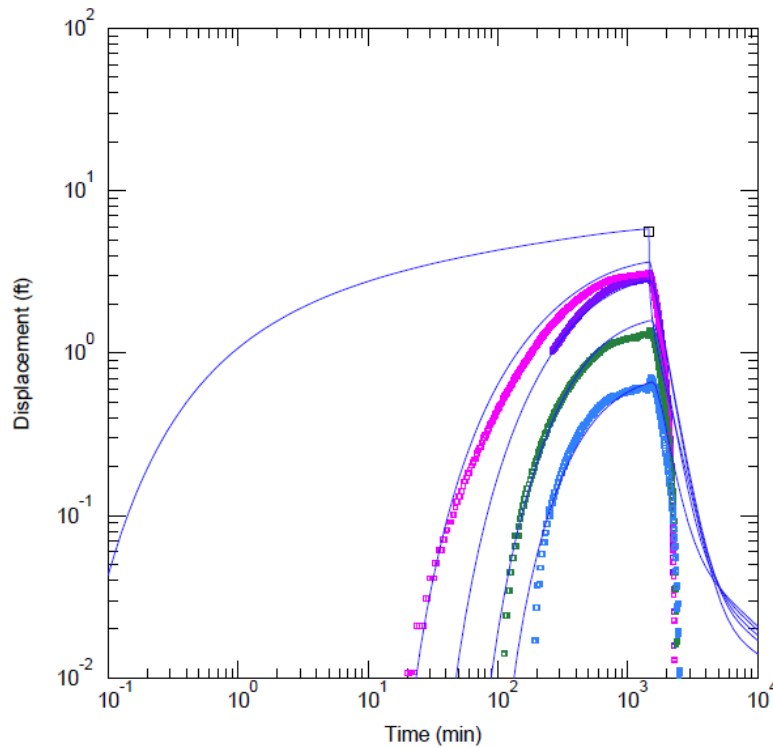


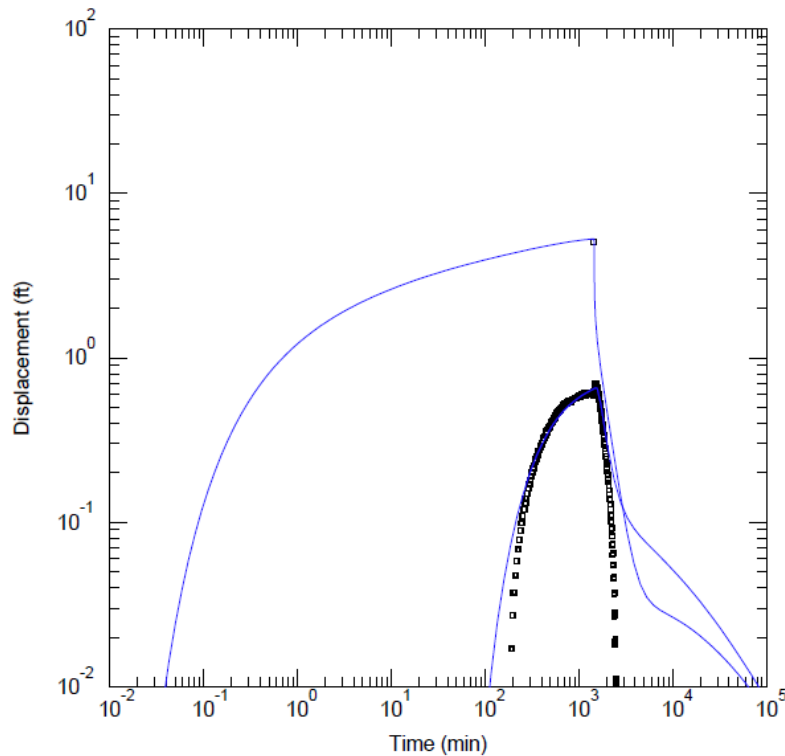
Figure 11. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B, 2-C, 2-D, and 2-E



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...11_cromwell_nest-2_neuman.aqt			Time: 15:08:21		
Date: 08/22/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>AQUIFER DATA</u>					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	□ Nest 2	0	50
			□ USGS 2-E	51.7	0
			□ USGS 2-D	46	0
			□ USGS 2-C	53.2	0
			□ USGS 2-B	54.8	0
<u>SOLUTION</u>					
Aquifer Model: <u>Leaky</u>			Solution Method: <u>Neuman-Witherspoon</u>		
T = 2200. ft ² /day			S = 0.0005		
1/B = 0.0017 ft ⁻¹			β/r = 0.0021 ft ⁻¹		
T2 = 10000. ft ² /day			S2 = 0.25		

L = 590 feet
 $kv = 130 * (0.0017)^2 * 2200 = 0.83 \text{ ft/day}$

Figure 12. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B only

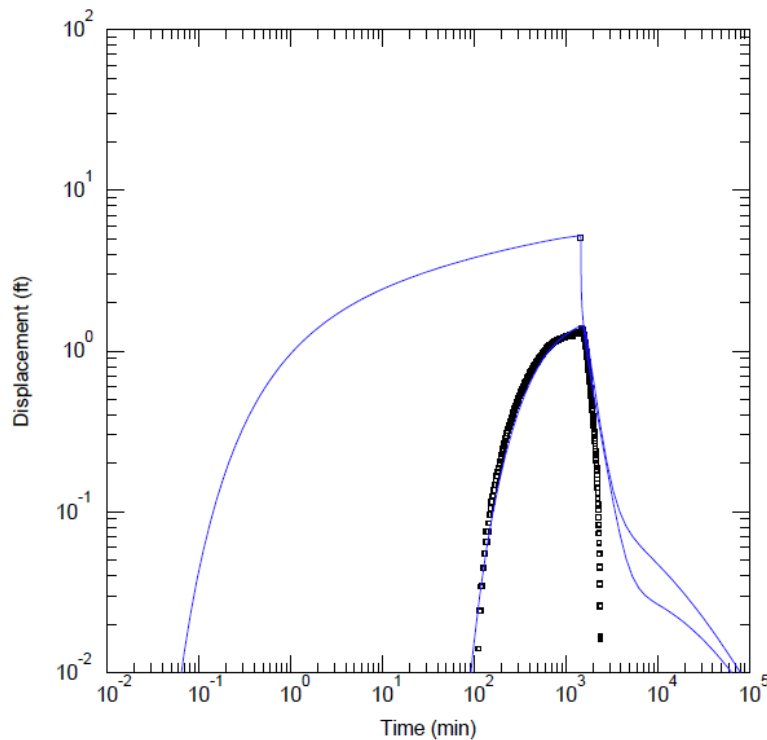


<u>WELL TEST ANALYSIS</u>					
Data Set: <u>O:\...\cromwell_nest-2_neuman_2B.aqt</u>			Time: <u>11:22:17</u>		
Date: <u>08/23/17</u>					
<u>PROJECT INFORMATION</u>					
Company: <u>MDH</u>					
Client: <u>City of Cromwell</u>					
Location: <u>Cromwell 4</u>					
Test Well: <u>C-4 (593593)</u>					
Test Date: <u>5/24/2017</u>					
<u>AQUIFER DATA</u>					
Saturated Thickness: <u>145. ft</u>			Anisotropy Ratio (Kz/Kr): <u>0.5</u>		
Aquitard Thickness (b'): <u>130. ft</u>			Aquitard Thickness (b''): <u>1. ft</u>		
<u>WELL DATA</u>					
<u>Pumping Wells</u>			<u>Observation Wells</u>		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	▫ Nest 2	0	50
			▫ USGS 2-B	54.8	0
<u>SOLUTION</u>					
Aquifer Model: <u>Leaky</u>			Solution Method: <u>Neuman-Witherspoon</u>		
T = <u>2300. ft²/day</u>			S = <u>0.0003</u>		
1/B = <u>0.002 ft⁻¹</u>			β/r = <u>0.0035 ft⁻¹</u>		
T2 = <u>2000. ft²/day</u>			S2 = <u>0.25</u>		

$$L = 500$$

$$kv = 130 * (0.002)^2 * 2300 = 1.2 \text{ ft/day}$$

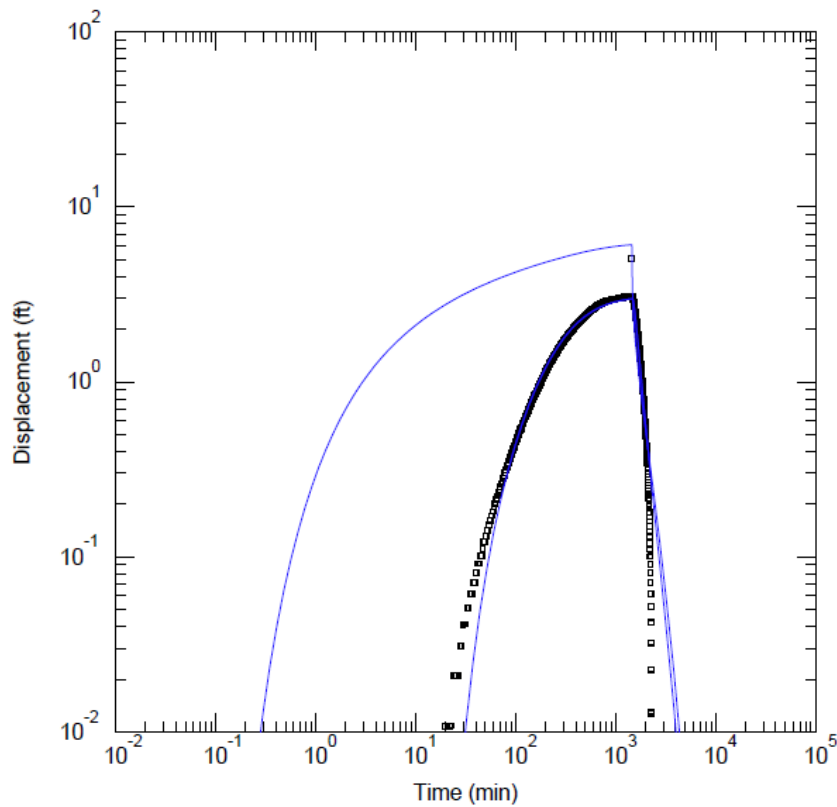
Figure 13. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B only



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...cromwell_nest-2_neuman_2C.aqt			Time: 11:23:18		
Date: 08/23/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>AQUIFER DATA</u>					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	▫ Nest 2	0	50
			▫ USGS 2-C	53.2	0
<u>SOLUTION</u>					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 2300. ft ² /day			S = 0.0005		
1/B = 0.002 ft ⁻¹			B/r = 0.003 ft ⁻¹		
T2 = 2000. ft ² /day			S2 = 0.25		

L = 500 Feet
 $k_v = 130 * (0.002)^2 * 2300 = 1.2 \text{ ft/day}$

Figure 14. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-C only

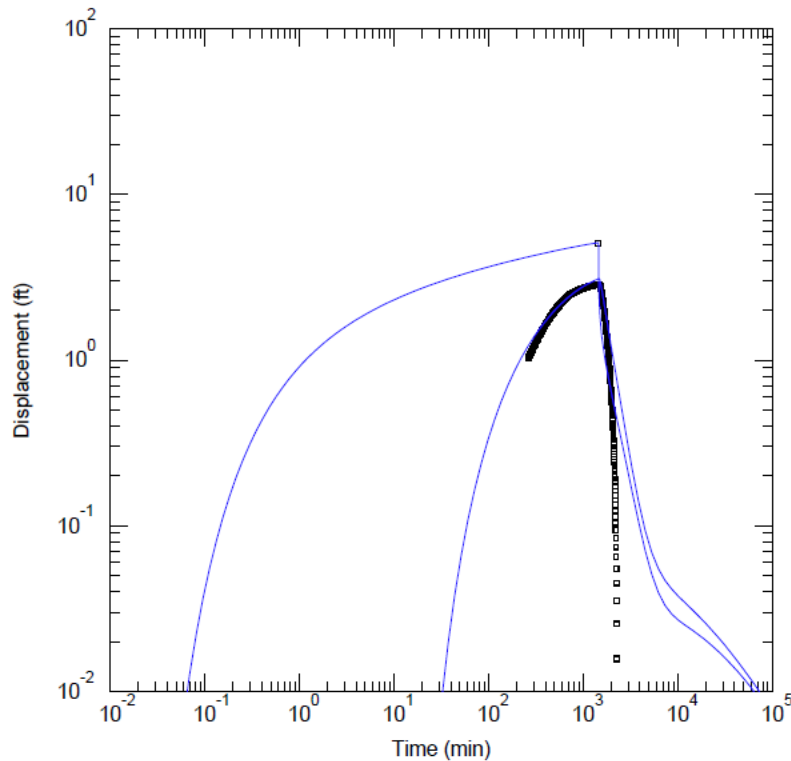


<u>WELL TEST ANALYSIS</u>					
Data Set: <u>O:\...cromwell_nest-2_neuman_2D.aqt</u>			Time: <u>11:24:59</u>		
Date: <u>08/23/17</u>					
<u>PROJECT INFORMATION</u>					
Company: <u>MDH</u>					
Client: <u>City of Cromwell</u>					
Location: <u>Cromwell 4</u>					
Test Well: <u>C-4 (593593)</u>					
Test Date: <u>5/24/2017</u>					
<u>AQUIFER DATA</u>					
Saturated Thickness: <u>145</u> ft			Anisotropy Ratio (Kz/Kr): <u>0.5</u>		
Aquitard Thickness (b'): <u>130</u> ft			Aquitard Thickness (b''): <u>1</u> ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	▣ Nest 2	0	50
			▣ USGS 2-D	46	0
<u>SOLUTION</u>					
Aquifer Model: <u>Leaky</u>			Solution Method: <u>Neuman-Witherspoon</u>		
T = <u>1800</u> ft ² /day			S = <u>0.001862</u>		
1/B = <u>0.002588</u> ft ⁻¹			β/r = <u>0.001745</u> ft ⁻¹		
T2 = <u>1.44E+8</u> ft ² /day			S2 = <u>1</u>		

L = 380 feet

$$kv = 130 * (0.00259)^2 * 1800 = 1.6 \text{ ft/day}$$

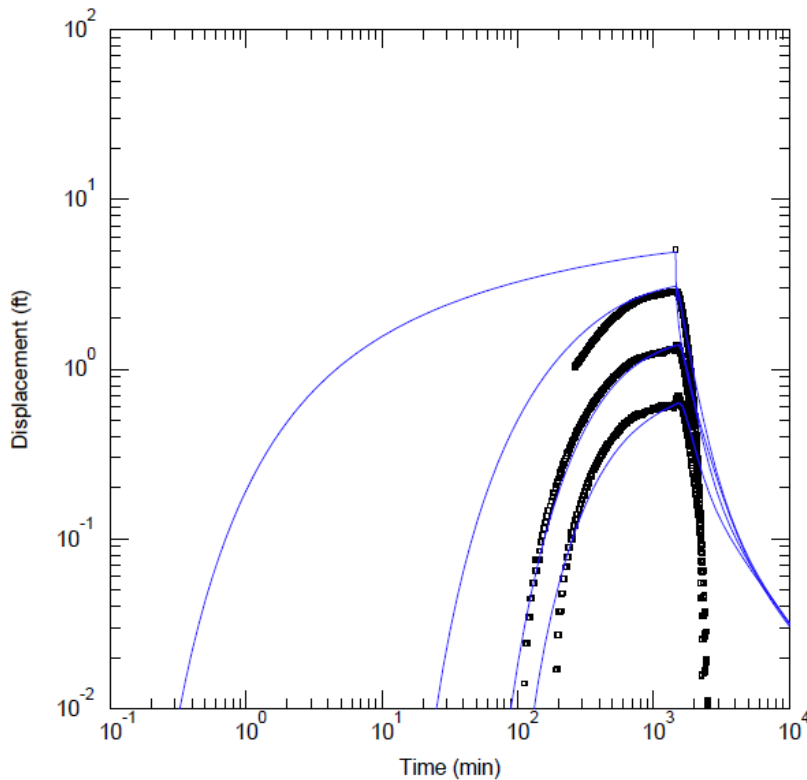
Figure 15. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-D only



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...\cromwell_nest-2_neuman_2E.aqt			Time: 11:26:03		
Date: 08/23/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>AQUIFER DATA</u>					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	• Nest 2	0	50
			• USGS 2-E	51.7	0
<u>SOLUTION</u>					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 2300. ft ² /day			S = 0.0005		
1/B = 0.002 ft ⁻¹			β/r = 0.0035 ft ⁻¹		
T2 = 2000. ft ² /day			S2 = 0.25		

L = 500 feet
 $kv = 130 * (0.002)^2 * 2300 = 1.2 \text{ ft/day}$

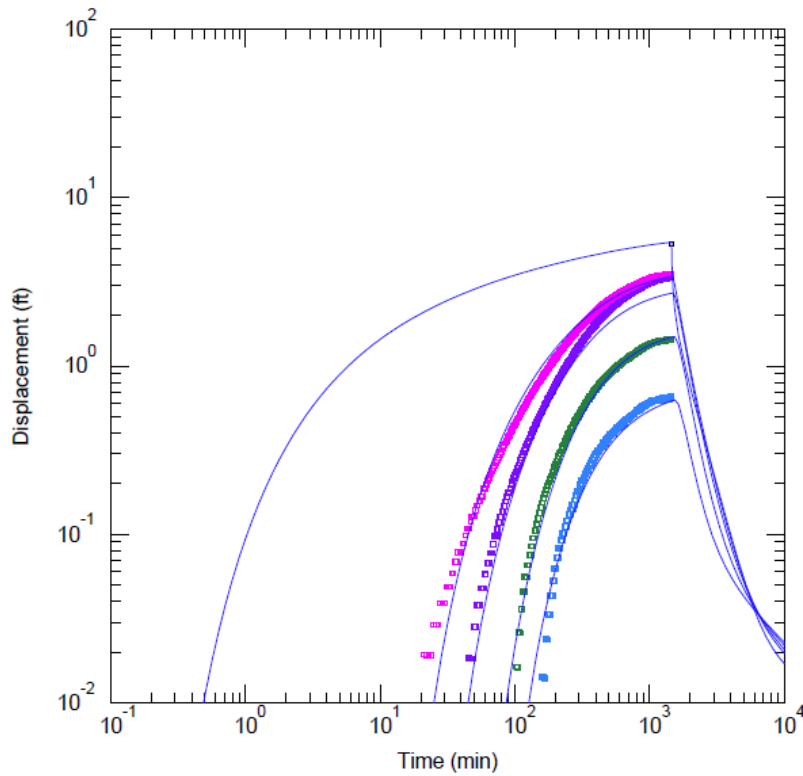
Figure 16. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B, 2-C, and 2-E only



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...\cromwell_nest-2_neuman_no2-D.aqt			Time: 14:45:40		
Date: 08/22/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>AQUIFER DATA</u>					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	▣ Nest 2	0	50
			▣ USGS 2-E	51.7	0
			▣ USGS 2-C	53.2	0
			▣ USGS 2-B	54.8	0
<u>SOLUTION</u>					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 2700. ft ² /day			S = 0.003		
1/B = 0.0015 ft ⁻¹			β/r = 0.0007 ft ⁻¹		
T2 = 10000. ft ² /day			S2 = 0.03		

L = 670 feet
 $kv = 130 * (0.0015)^2 * 2700 = 0.79 \text{ ft/day}$

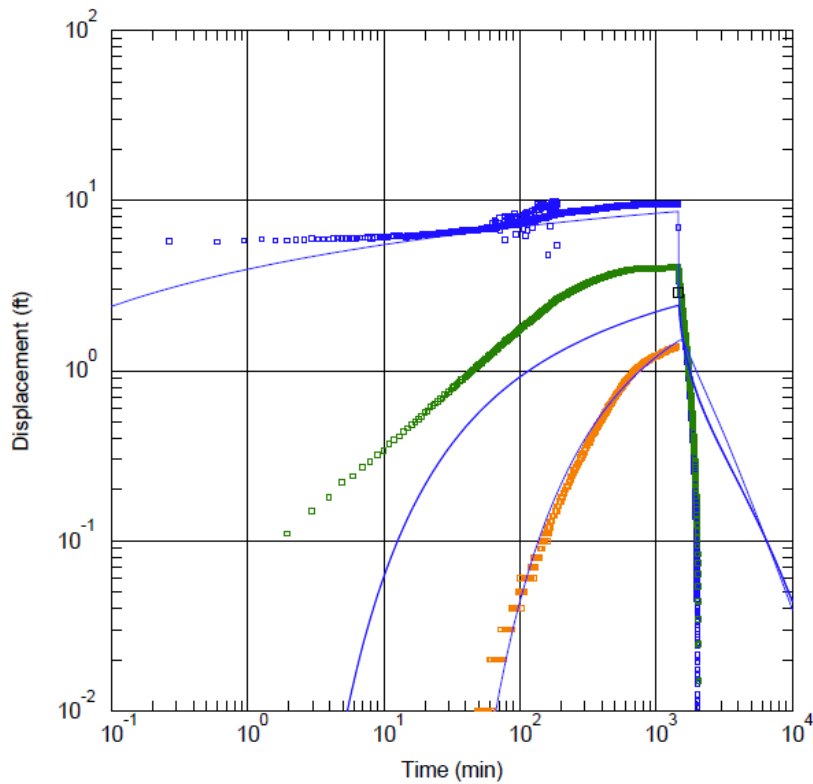
Figure 17. Solution of Aquifer Properties by Aqtesolv. Recovery Phase Data from USGS 2-B, 2-C, 2-D, and 2-E



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...cromwell_nest-2_neuman_no2-D_recovery.aqt					
Date: 08/21/17			Time: 08:14:53		
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>AQUIFER DATA</u>					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	Nest 2	0	50
			USGS 2-E	51.7	0
			USGS 2-C	53.2	0
			USGS 2-B	54.8	0
			USGS 2-D	46	0
<u>SOLUTION</u>					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 2300. ft ² /day			S = 0.004		
1/B = 0.0017 ft ⁻¹			B/r = 0.0007 ft ⁻¹		
T2 = 10000. ft ² /day			S2 = 0.2		

L = 590 feet
 $kv = 130 * (0.0017)^2 * 2300 = 0.86 \text{ ft/day}$

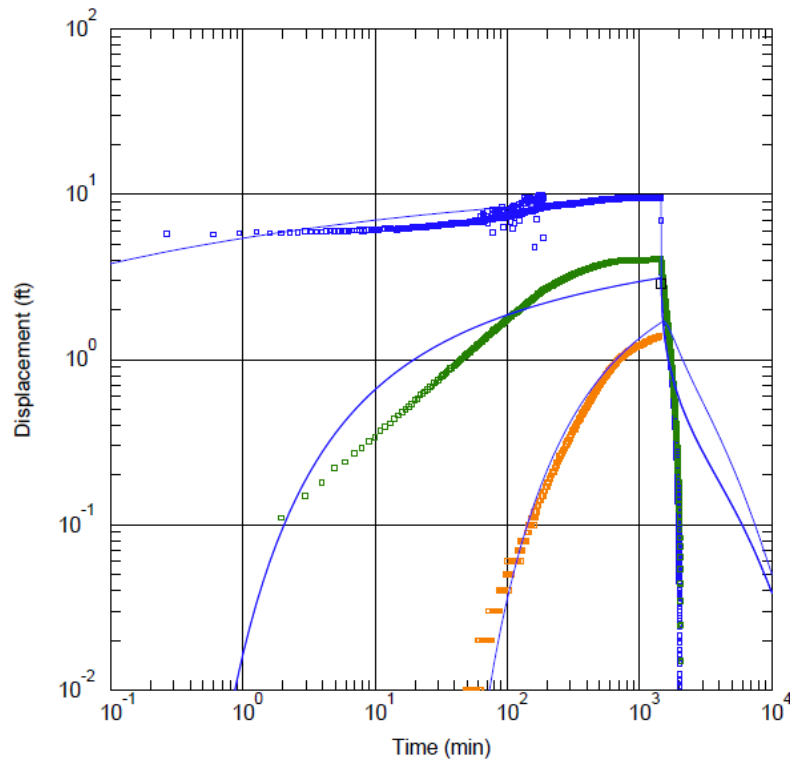
Figure 18. Solution of Aquifer Properties by Aqtesolv. Match to Data from USGS 1-A, Data from USGS 1-B, and Cromwell 4



WELL TEST ANALYSIS					
Data Set: O:\...\cromwell_nest-1_neuman.aqt			Time: 15:14:42		
Date: 08/22/17					
PROJECT INFORMATION					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
AQUIFER DATA					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
WELL DATA					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	■ Cromwell 4	0	0
			■ 1-B	140.5	0
			■ 1-A	142	0
			■ Nest 1	141	0
SOLUTION					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 3731.6 ft ² /day			S = 0.008047		
1/B = 0.0006568 ft ⁻¹			B/r = 0.0001826 ft ⁻¹		
T2 = 1.44E+8 ft ² /day			S2 = 1.		

L = 1520 feet
 $kv = 130 * (0.00066)^2 * 3730 = 0.21 \text{ ft/day}$

Figure 19. Solution of Aquifer Properties by Aqtesolv. Match to Data from USGS 1-A and Modeled Drawdown at the Base of Till, Data from USGS 1-B, and Cromwell 4

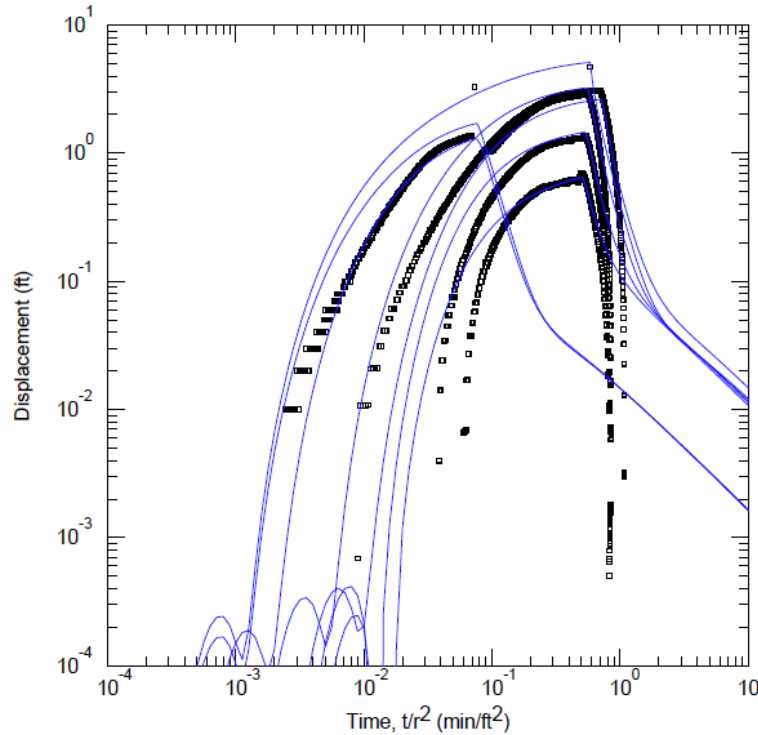


WELL TEST ANALYSIS					
Data Set: O:\...\cromwell_nest-1_neuman_obws_only.aqt					
Date: 08/22/17			Time: 09:35:30		
PROJECT INFORMATION					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
AQUIFER DATA					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
WELL DATA					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	■ Cromwell 4	0	0
			■ 1-B	140.5	0
			■ 1-A	142	0
			□ Nest 1	141	0
SOLUTION					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 3547.8 ft ² /day			S = 0.001231		
1/B = 0.0005151 ft ⁻¹			β/r = 0.0003916 ft ⁻¹		
T2 = 2000. ft ² /day			S2 = 0.3		

L = 1960 feet

kv = 130 * (0.00051)^2 * 3550 = 0.12 ft/day

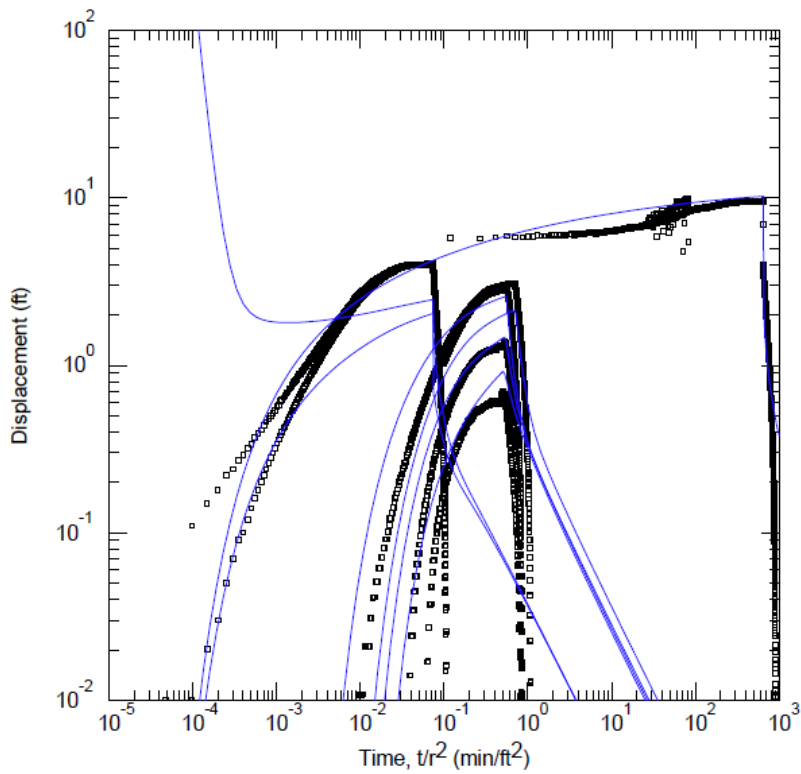
Figure 20. Solution of Aquifer Properties by Aqtesolv. Match to Data from all USGS Observation Wells and Drawdown at the Base of Till at Nests 1 and 2



WELL TEST ANALYSIS					
Data Set: O:\...15_cromwell_nests1&2_neuman.aqt			Time: 15:22:35		
Date: 08/22/17					
PROJECT INFORMATION					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
AQUIFER DATA					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 0.5		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 1. ft		
WELL DATA					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
4	0	0	▣ Nest 2	0	50
			▣ USGS 2-E	51.7	0
			▣ USGS 2-D	46	0
			▣ USGS 2-C	53.2	0
			▣ USGS 2-B	54.8	0
			▣ USGS 1-A	142	0
			▣ Nest 1	140.5	0
SOLUTION					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 1204.1 ft ² /day			S = 0.02603		
1/B = 0.006891 ft ⁻¹			B/r = 0.001982 ft ⁻¹		
T2 = 10000. ft ² /day			S2 = 1.		

L = 145 feet
 $kv = 130 * (0.00689)^2 * 1200 = 7.4 \text{ ft/day}$

Figure 21. Solution of Aquifer Properties by Aqtesolv. Match to all data



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...cromwell4_neuman_composite_thick.aqt			Time: 13:22:20		
Date: 08/21/17					
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>AQUIFER DATA</u>					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 1.		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 20. ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	□ Cromwell 4	0	0
			□ 1-B	140.5	0
			□ 1-C	140.4	0
			□ 2-B	0	54.8
			□ 2-C	0	53.2
			□ 2-D	0	46
			□ 2-E	0	51.7
<u>SOLUTION</u>					
Aquifer Model: Leaky			Solution Method: Neuman-Witherspoon		
T = 2785.3 ft ² /day			S = 0.00291		
1/B = 0.002969 ft ⁻¹			B/r = 0.002176 ft ⁻¹		
T2 = 2200. ft ² /day			S2 = 0.03		

Figure 22. Similarity in Slope of 1-A and 2-E

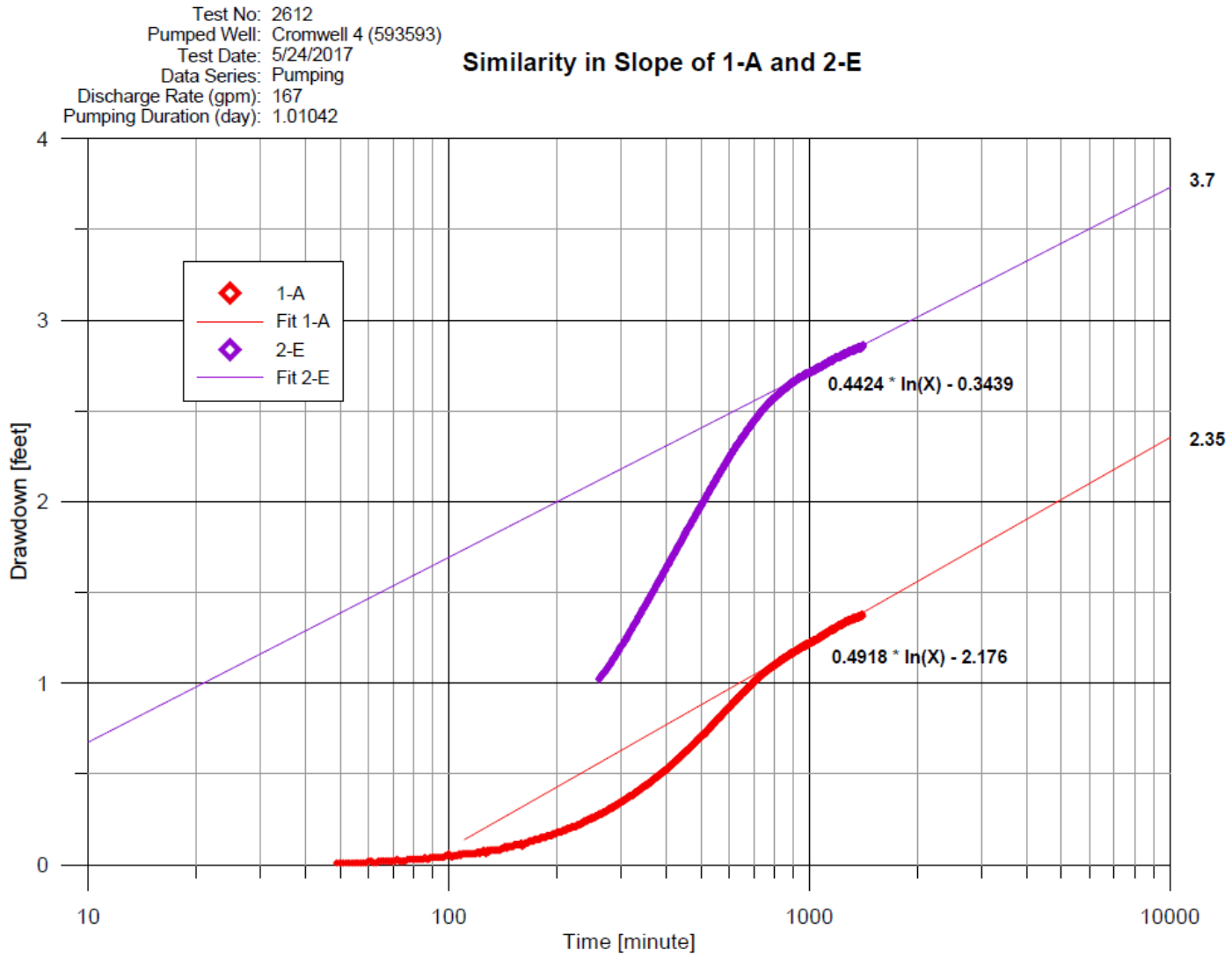
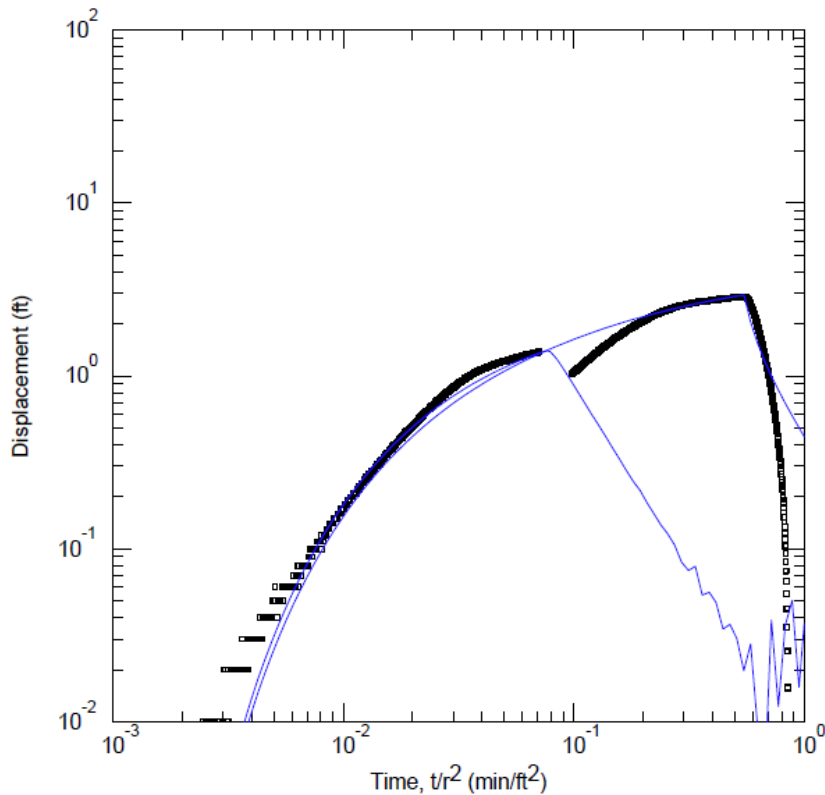


Figure 23. Solution of Aquifer Properties by Aqtesolv. Match to Data from USGS 1-A and USGS 2-E



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...124_cromwell4_1-A&2-E_neuman_composite.aqt					
Date: <u>09/12/17</u>			Time: <u>14:03:19</u>		
<u>PROJECT INFORMATION</u>					
Company: <u>MDH</u>					
Client: <u>City of Cromwell</u>					
Location: <u>Cromwell 4</u>					
Test Well: <u>C-4 (593593)</u>					
Test Date: <u>5/24/2017</u>					
<u>AQUIFER DATA</u>					
Saturated Thickness: <u>145. ft</u>			Anisotropy Ratio (Kz/Kr): <u>1.</u>		
Aquitard Thickness (b'): <u>130. ft</u>			Aquitard Thickness (b''): <u>20. ft</u>		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	□ 1-A	140.6	0
			□ 2-E	0	51.7
<u>SOLUTION</u>					
Aquifer Model: <u>Leaky</u>			Solution Method: <u>Neuman-Witherspoon</u>		
T = <u>1589. ft²/day</u>			S = <u>0.05497</u>		
1/B = <u>0.004471 ft⁻¹</u>			β/r = <u>7.276E-8 ft⁻¹</u>		
T2 = <u>10000. ft²/day</u>			S2 = <u>0.3</u>		

L = 224 feet
 $kv = 130 * (0.00447)^2 * 1590 = 4.1 \text{ ft/day}$

Figure 24. Agarwal Analysis

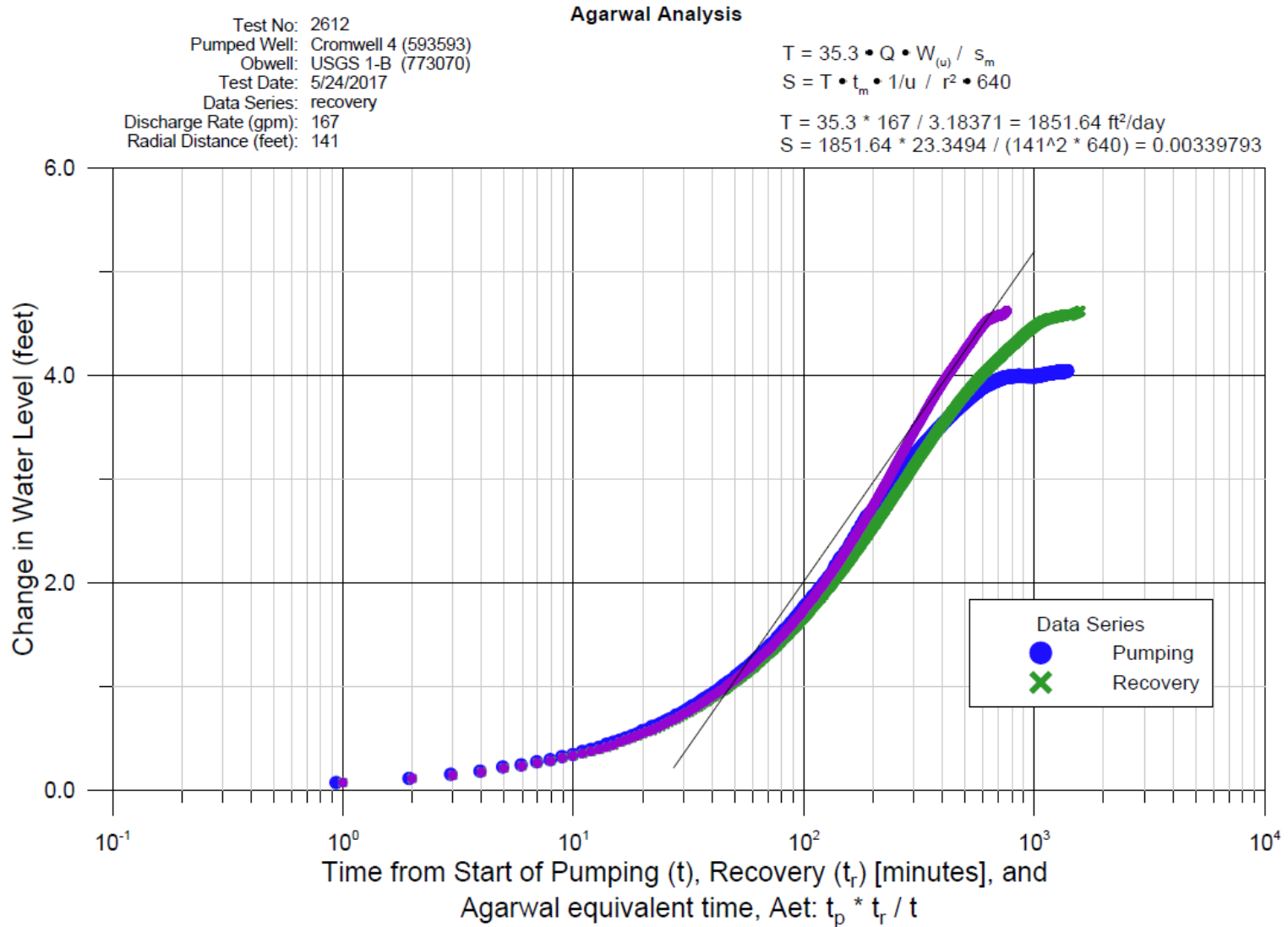
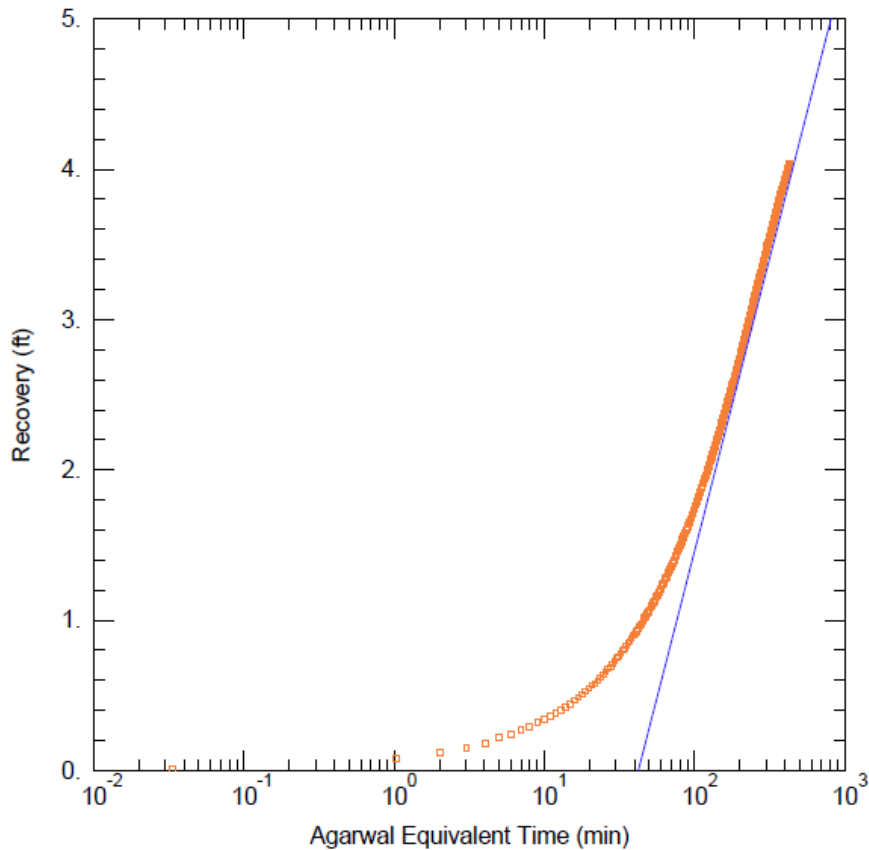


Figure 25. Solution of Aquifer Properties by Aqtesolv. Analysis of Recovery Data from Pumped Well



<u>WELL TEST ANALYSIS</u>					
Data Set: <u>O:\...\cromwell-4_nest-1-B_agarwal_theis.aqt</u>			Time: <u>16:43:05</u>		
Date: <u>09/06/17</u>					
<u>PROJECT INFORMATION</u>					
Company: <u>MDH</u>					
Client: <u>City of Cromwell</u>					
Location: <u>Cromwell 4</u>					
Test Well: <u>C-4 (593593)</u>					
Test Date: <u>5/24/2017</u>					
<u>AQUIFER DATA</u>					
Saturated Thickness: <u>145</u> ft			Anisotropy Ratio (Kz/Kr): <u>1</u>		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	1-B	140.5	0
<u>SOLUTION</u>					
Aquifer Model: <u>Confined</u>			Solution Method: <u>Cooper-Jacob</u>		
T = <u>1511.4</u> ft ² /day			S = <u>0.00504</u>		

Figure 26. Well Identification

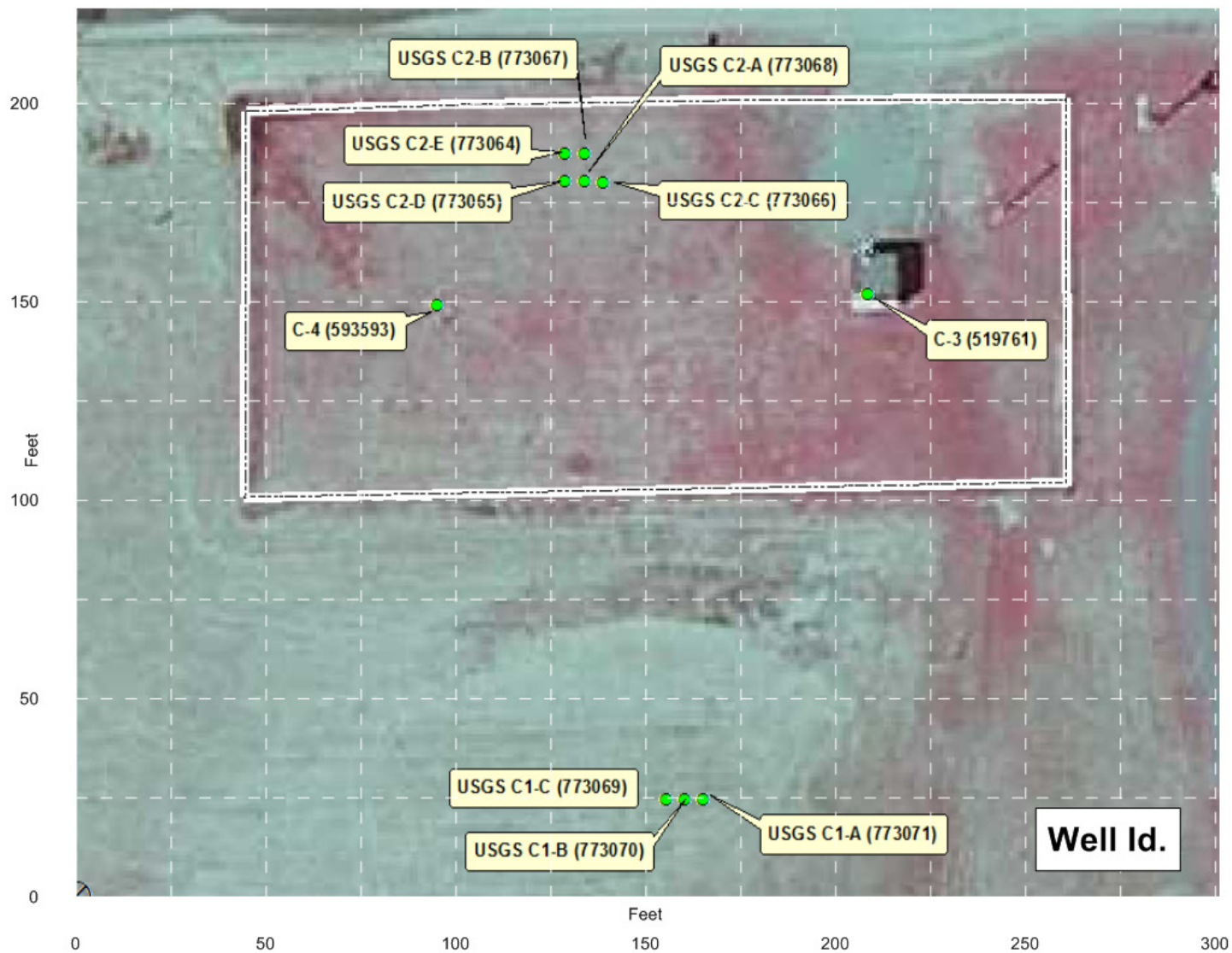


Figure 27. Distances between Wells and Well Nests

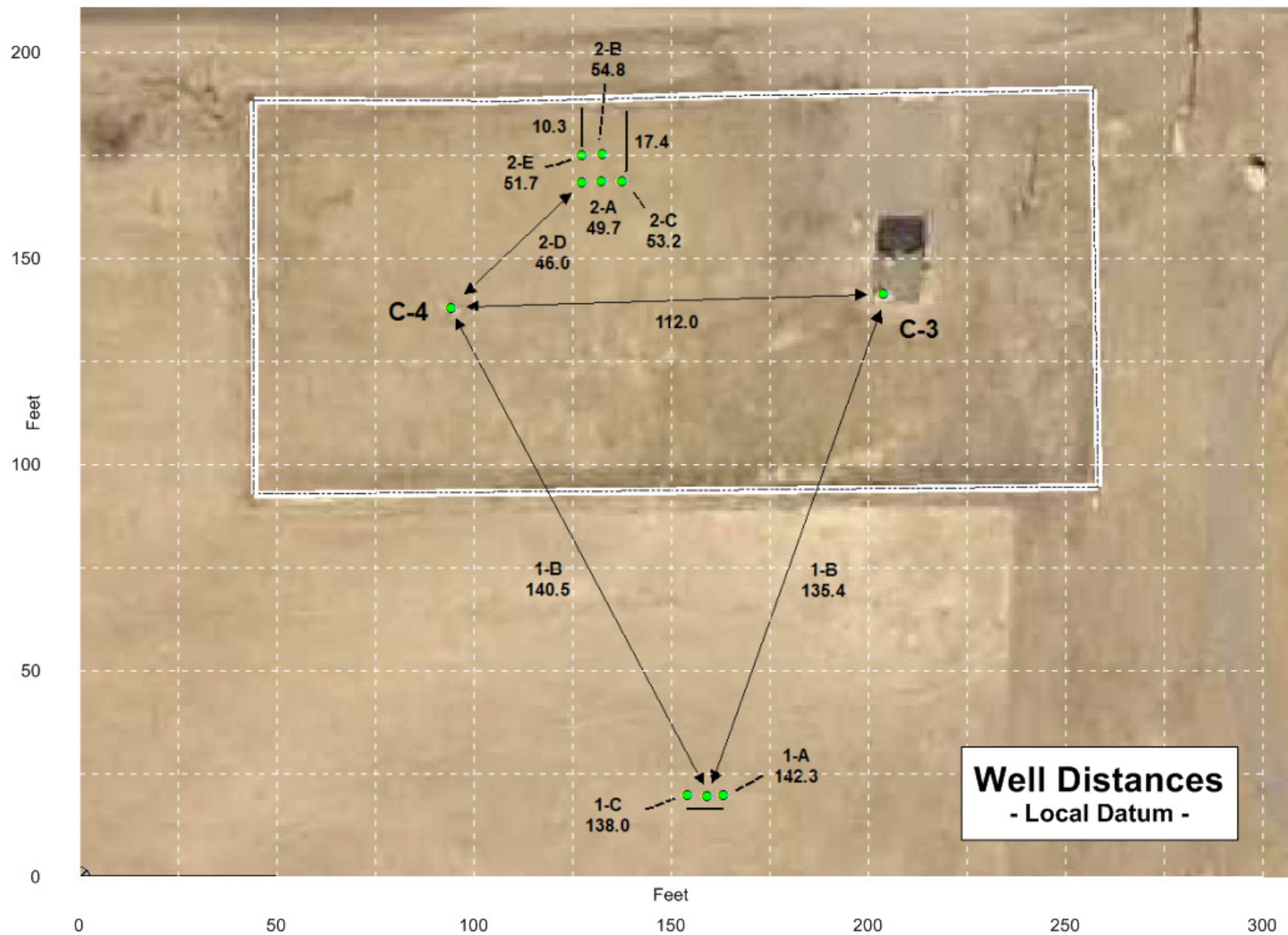
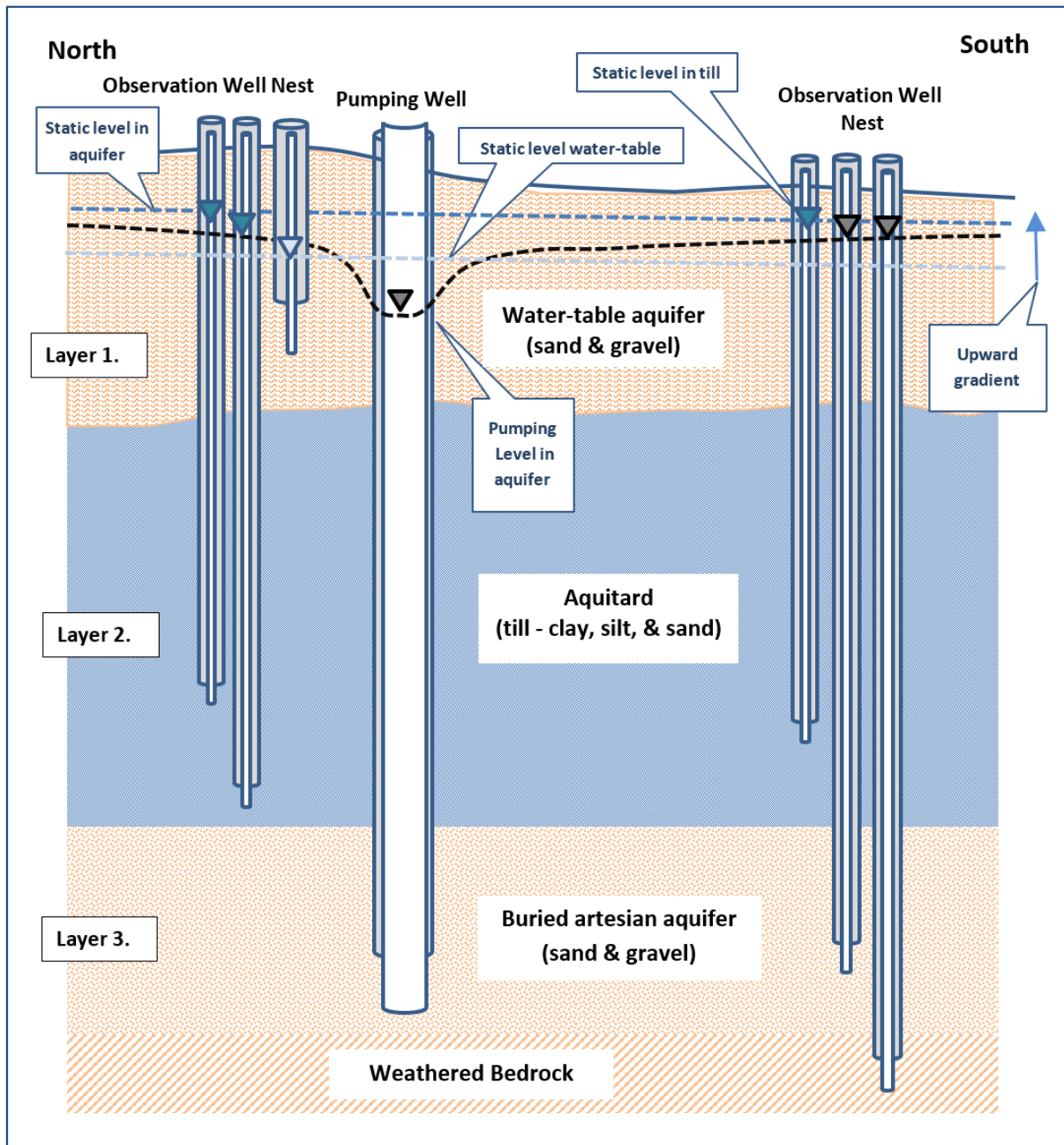


Figure 28. Schematic Section Across Site



Schematic Section

Figure 29. Time-series of Groundwater Elevation Collected at Cromwell 4.

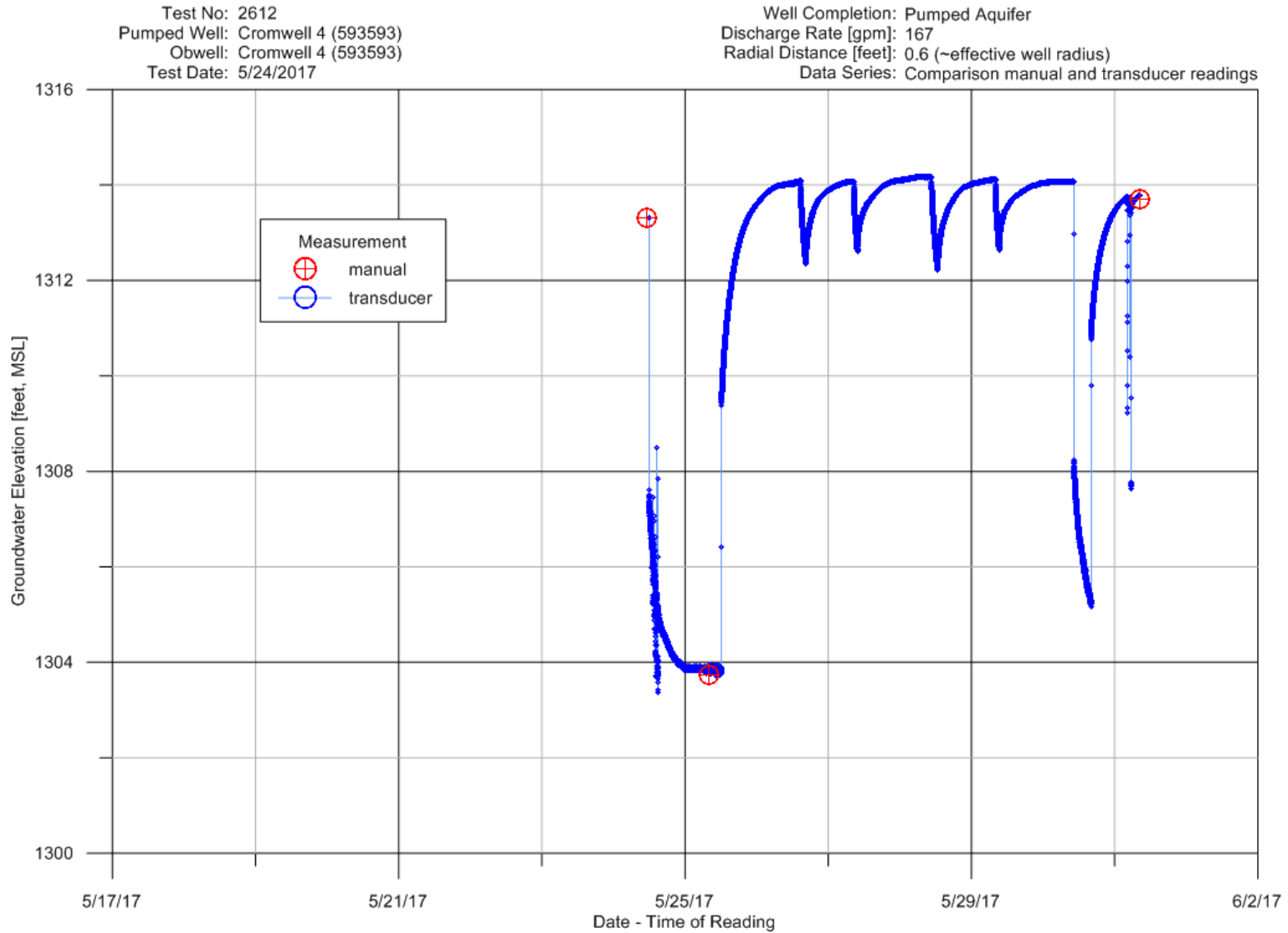


Figure 30. Time-series of Groundwater Elevation Collected at USGS 1-A.

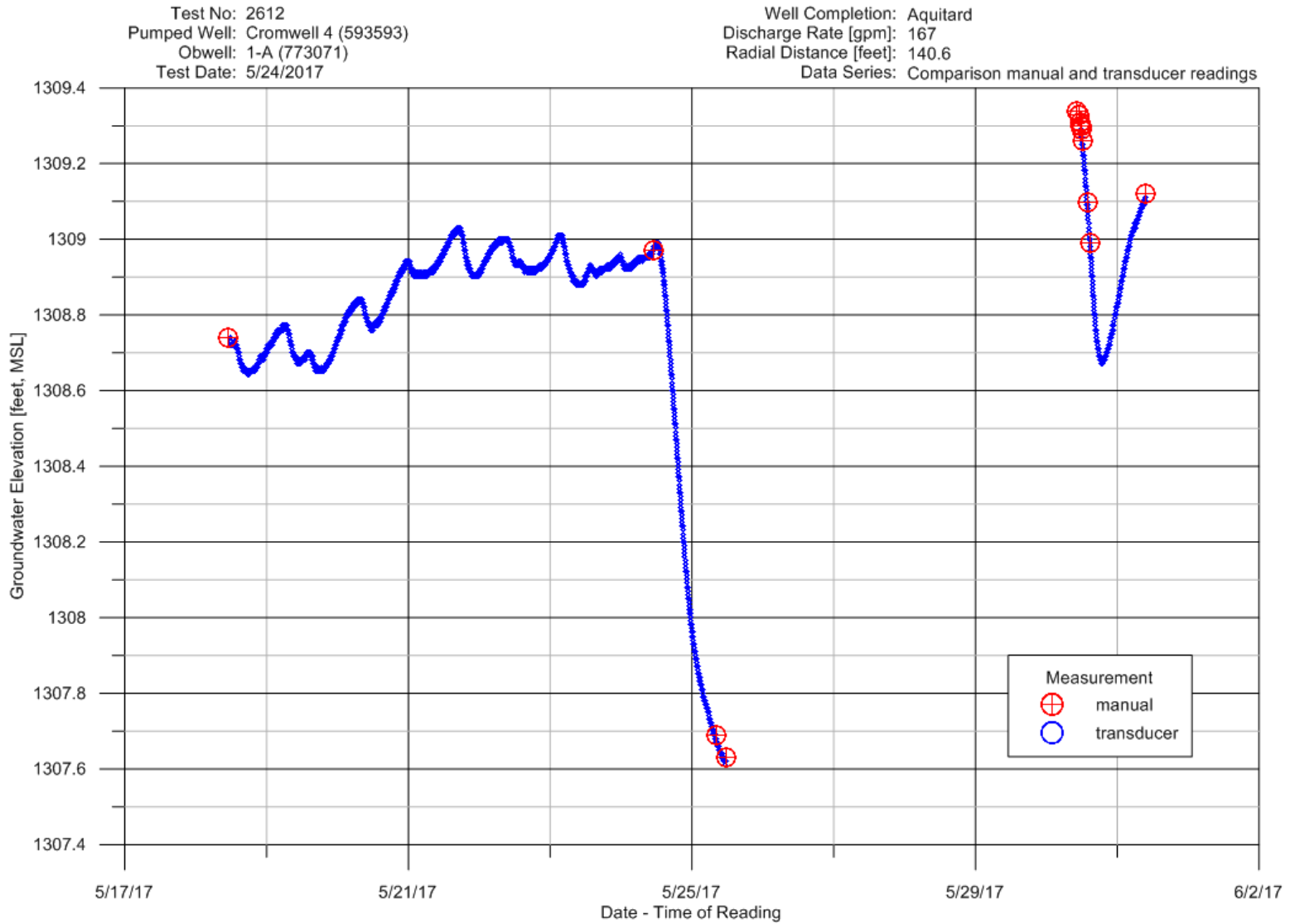


Figure 31. Time-series of Groundwater Elevation Collected at USGS 1-B

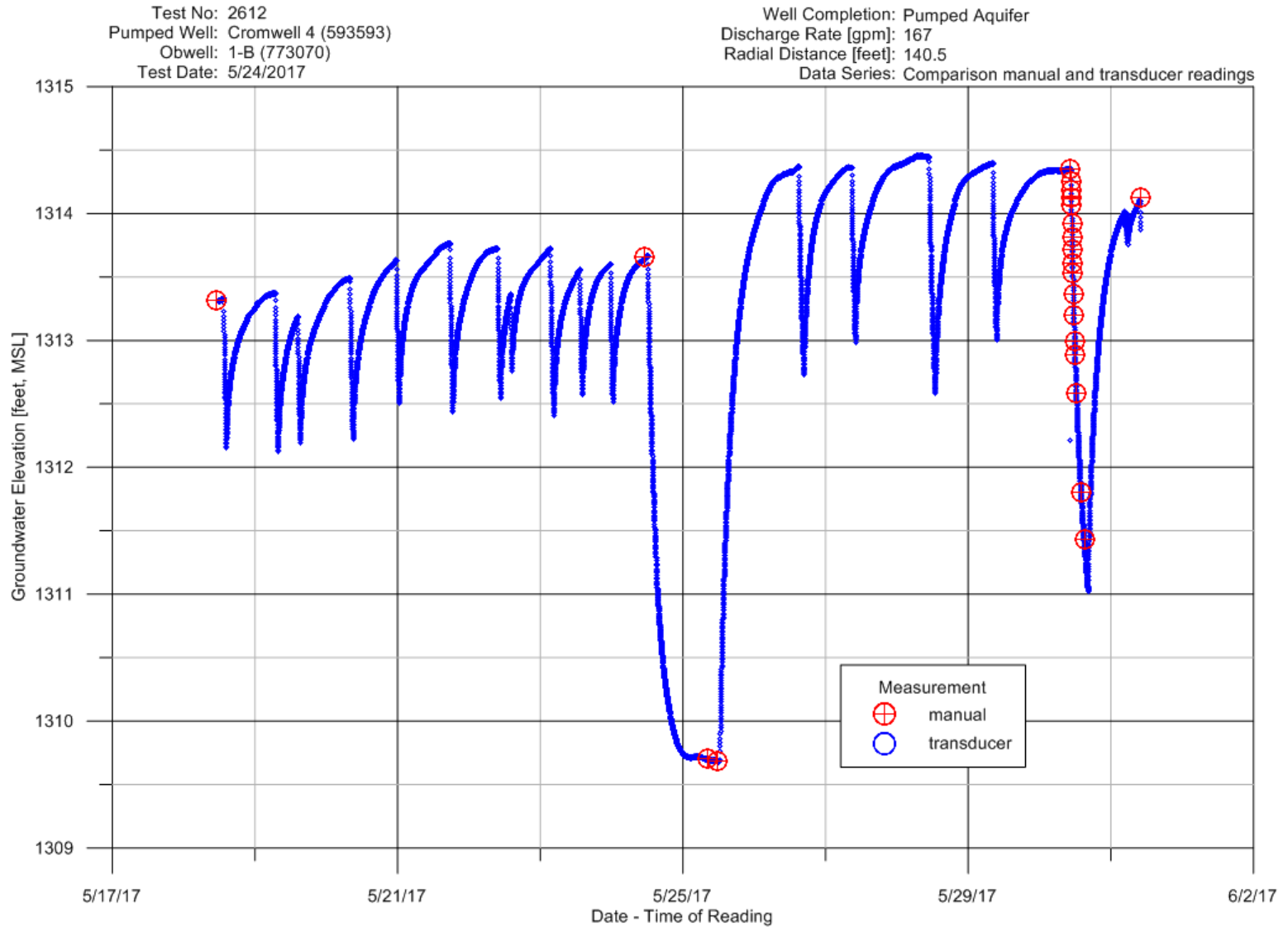


Figure 32. Time-series of Groundwater Elevation Collected at USGS 1-C

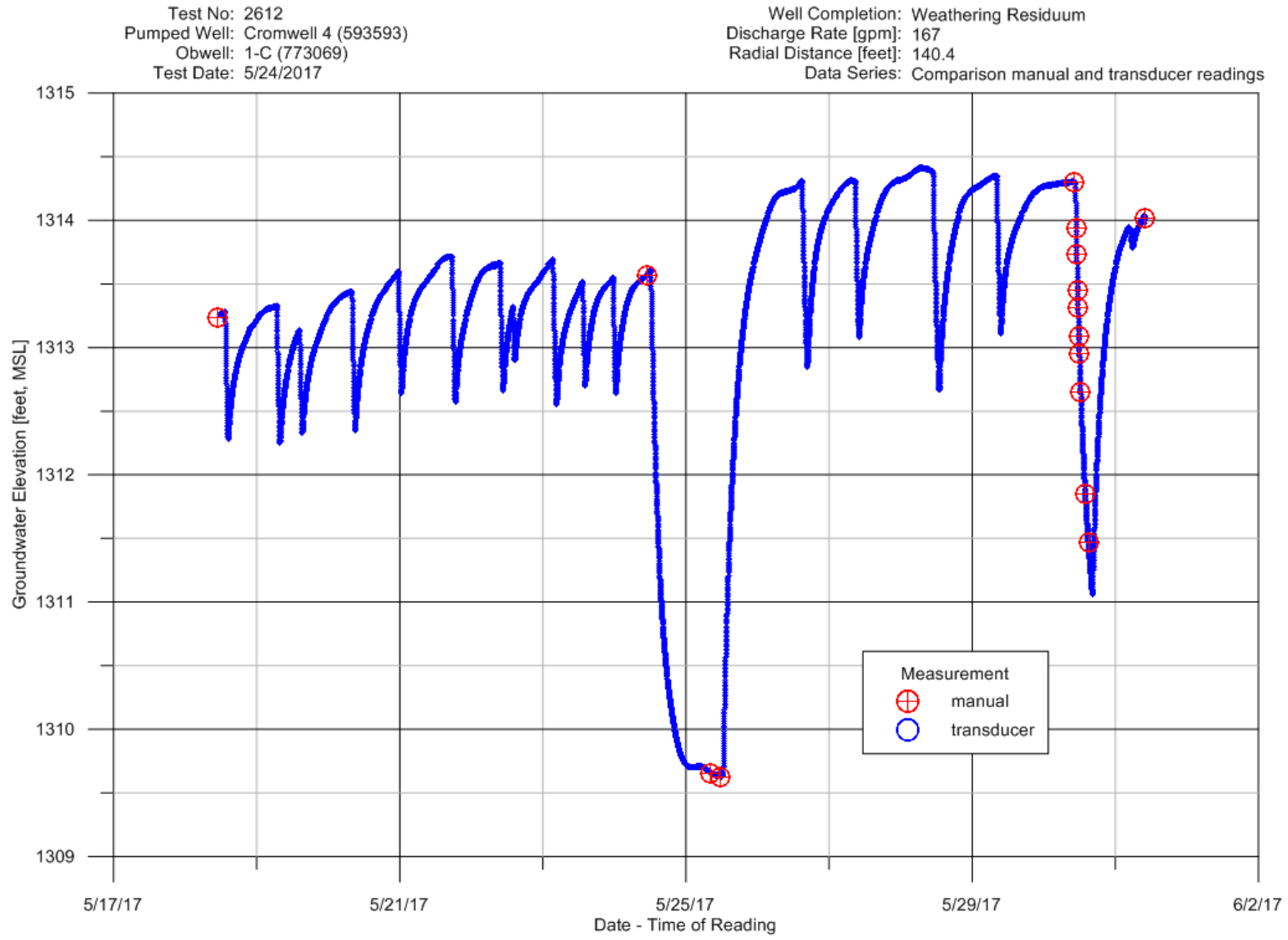


Figure 33. Time-series of Groundwater Elevation Collected at USGS 2-A

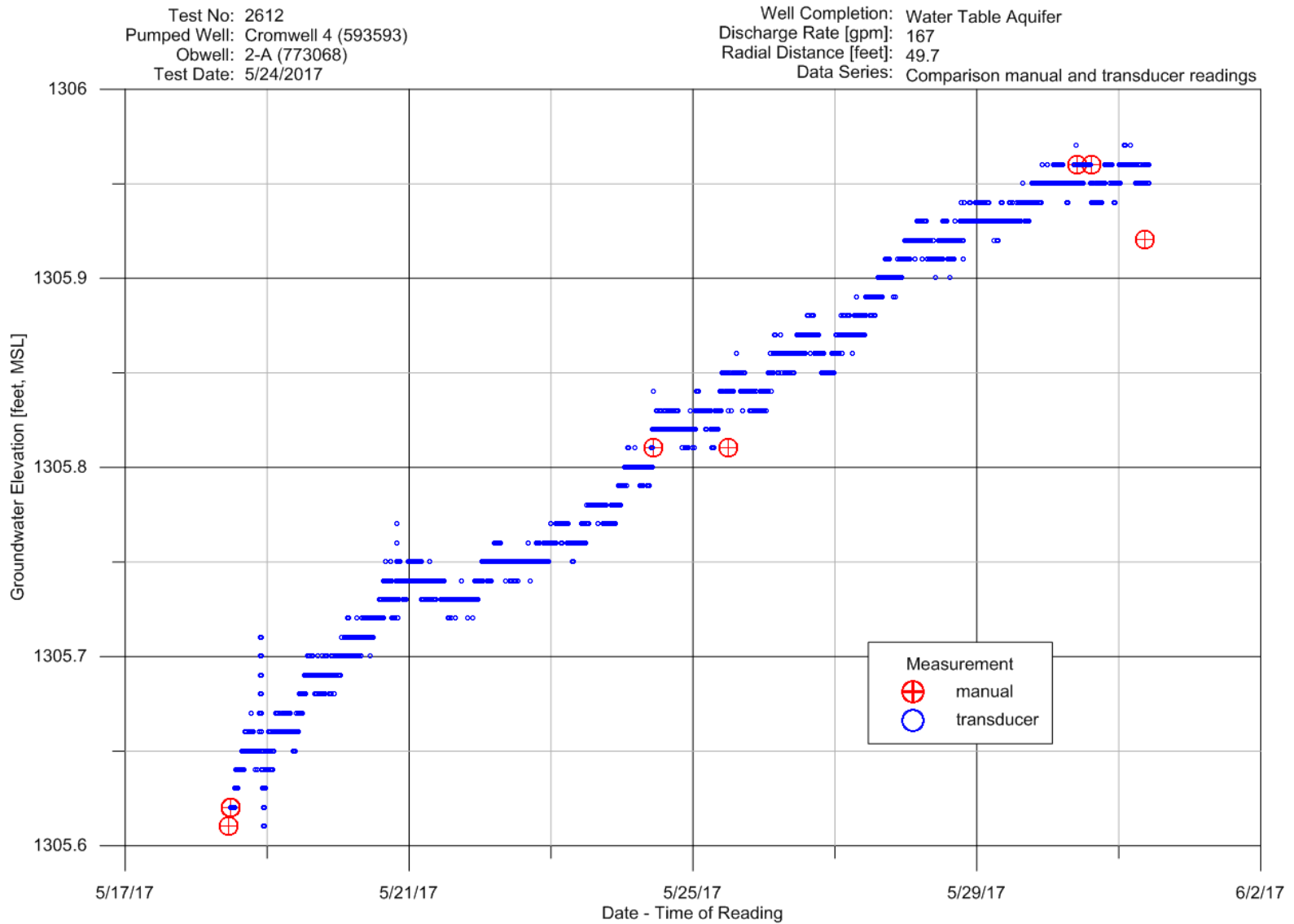


Figure 34. Time-series of Groundwater Elevation Collected at USGS 2-B

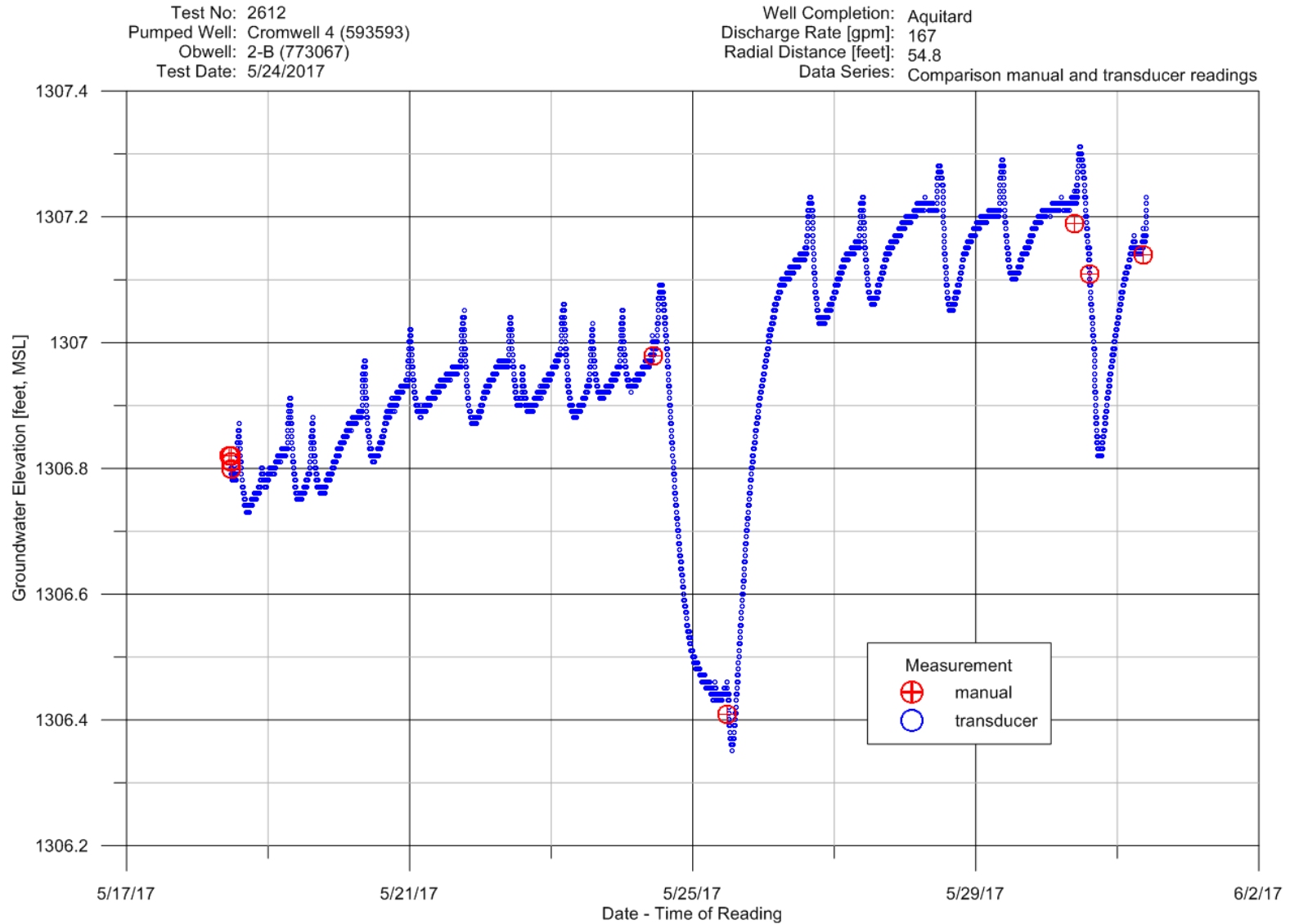


Figure 35. Time-series of Groundwater Elevation Collected at USGS 2-C

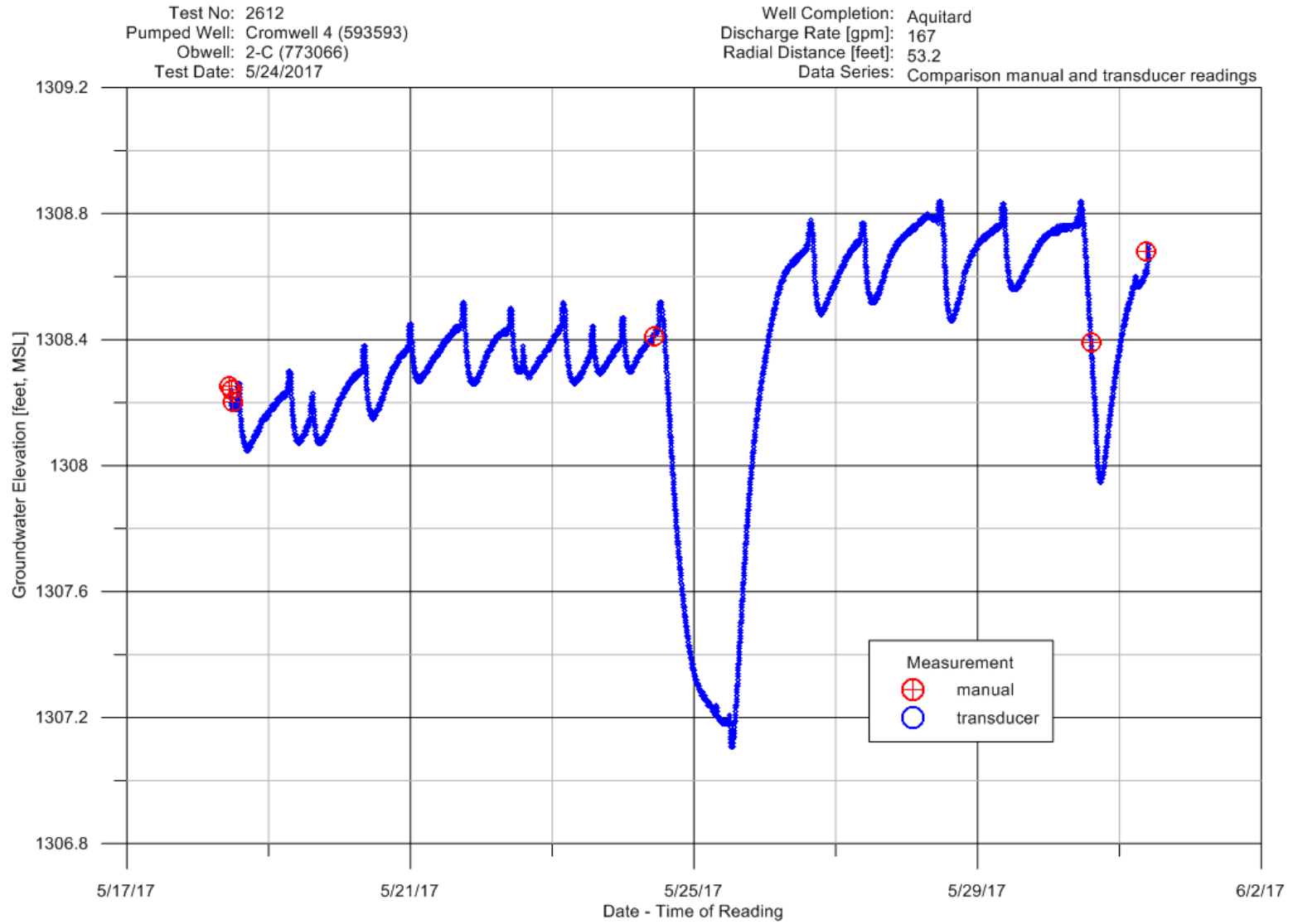


Figure 37. Time-series of Groundwater Elevation Collected at USGS 2-E

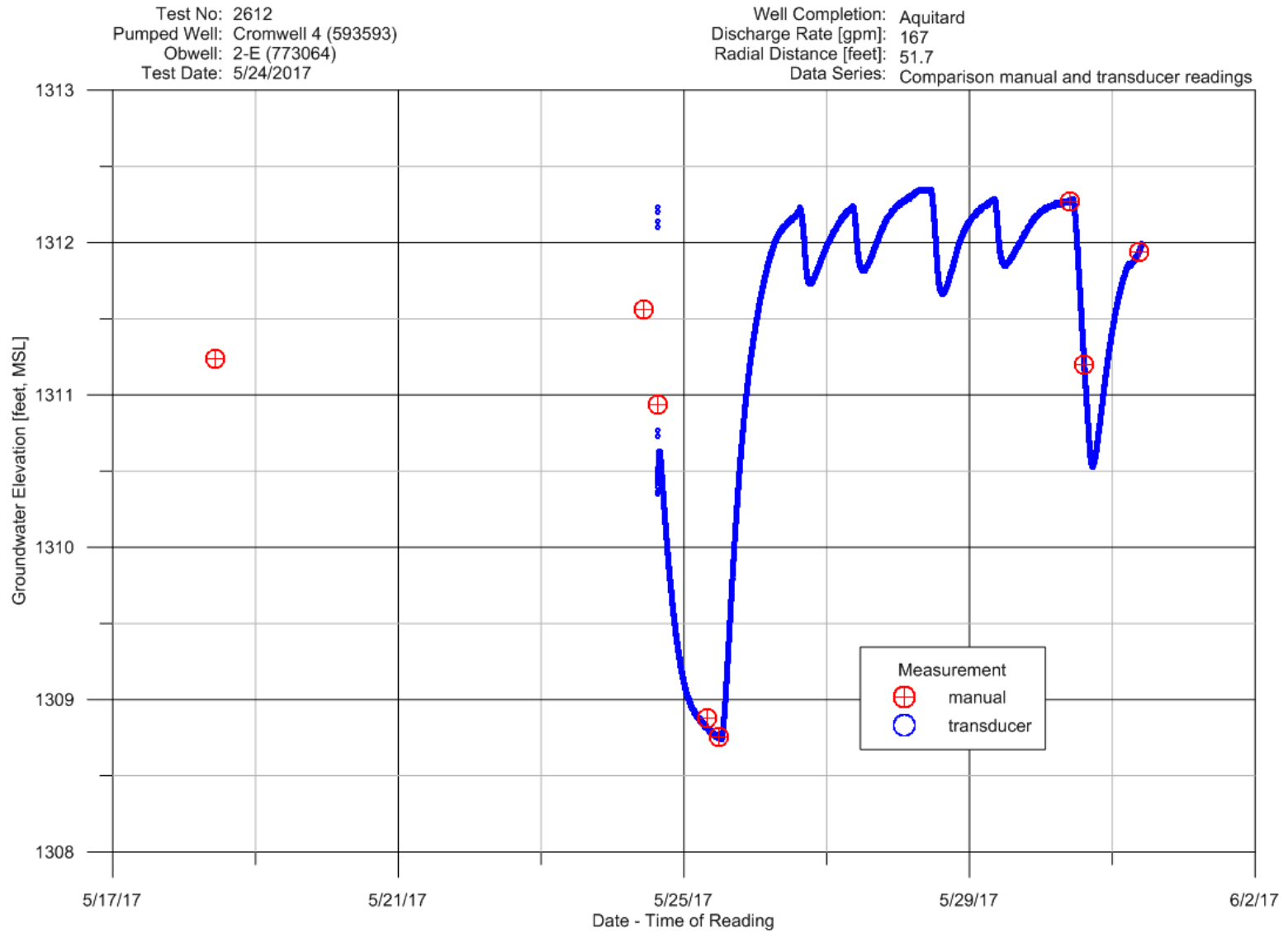


Figure 38. Time-series of Groundwater Elevation Collected at all Wells

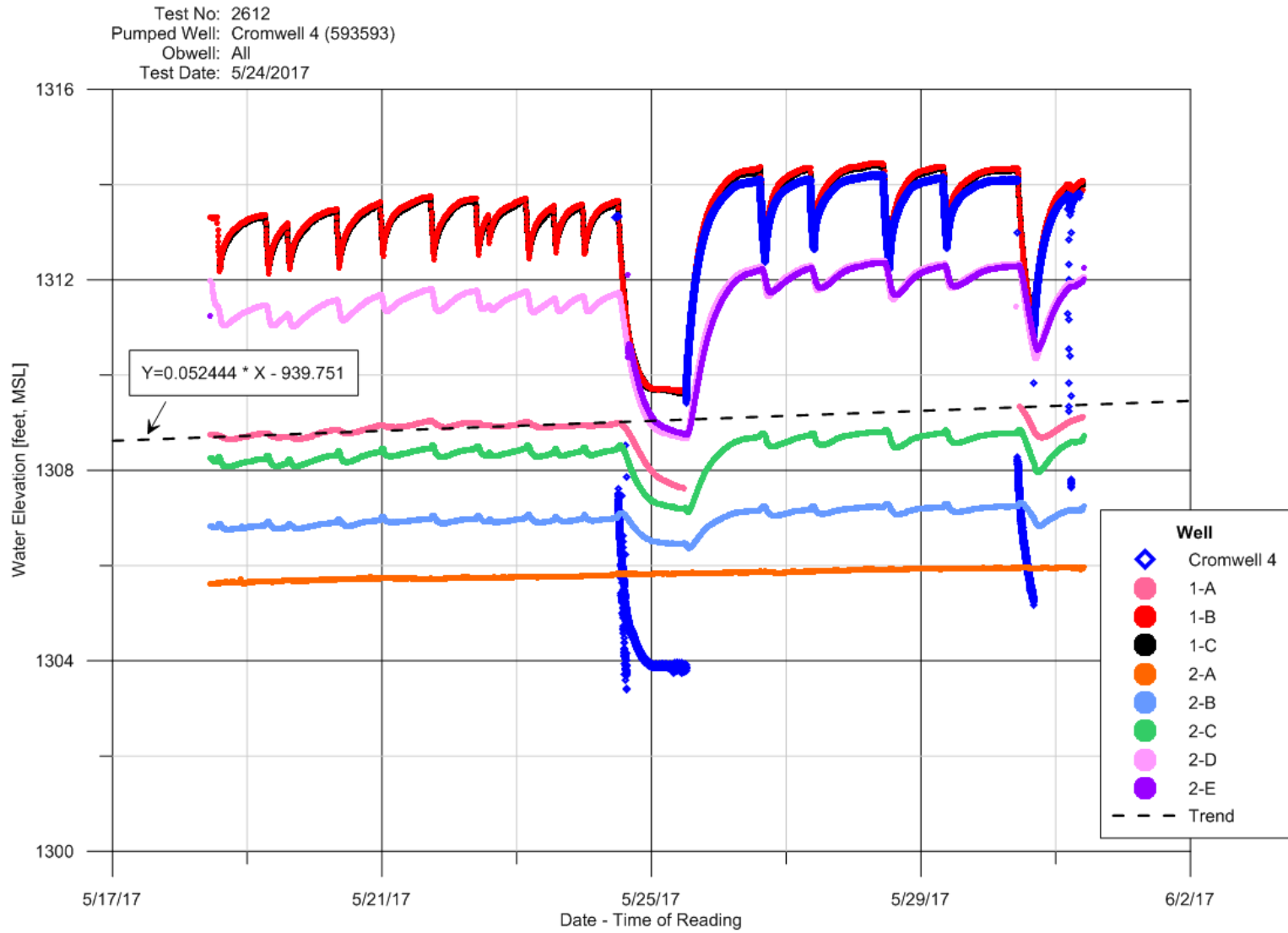


Figure 39. Time-series of Groundwater Elevation Collected at Cromwell 4 and Nest 1

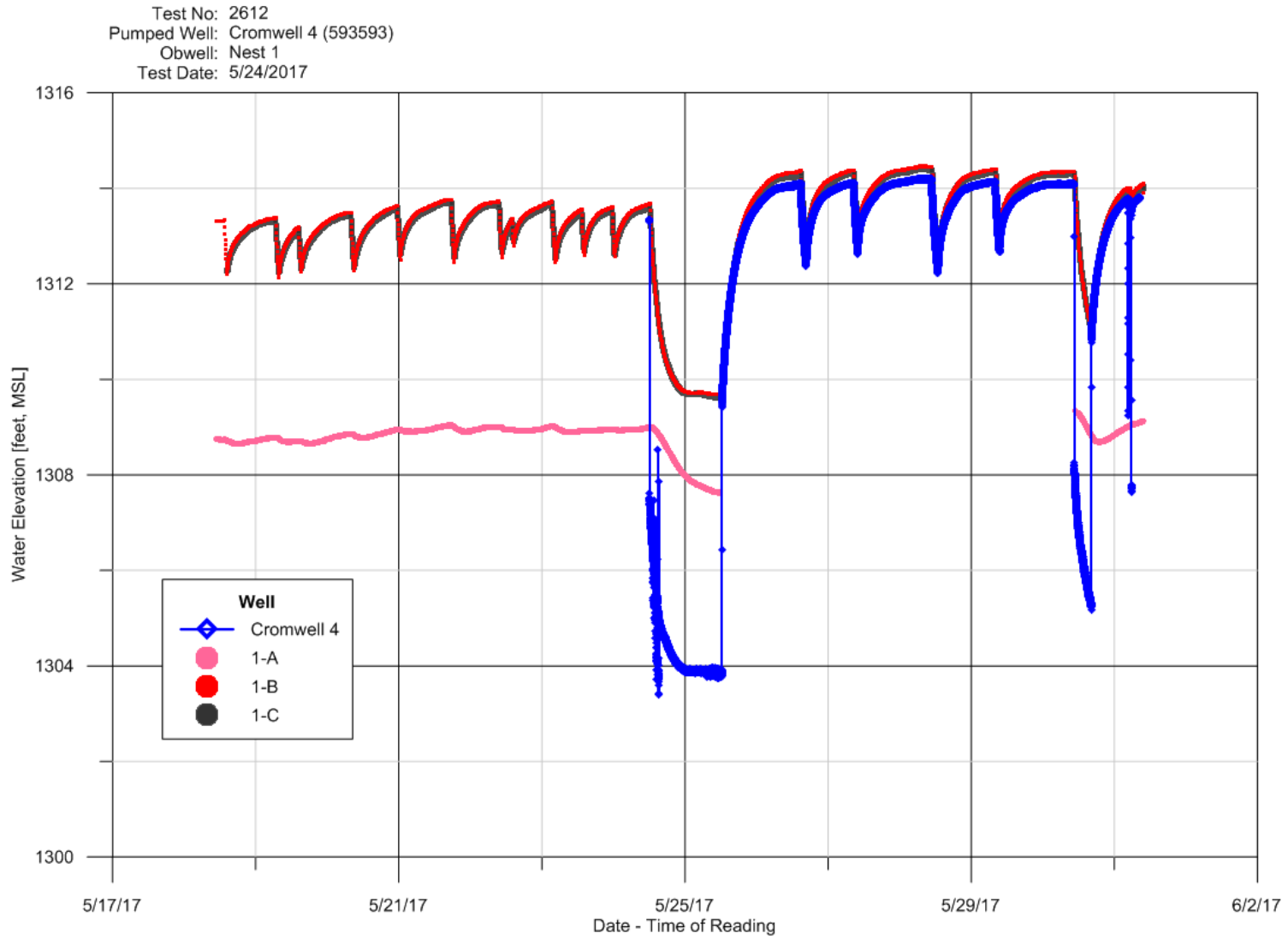
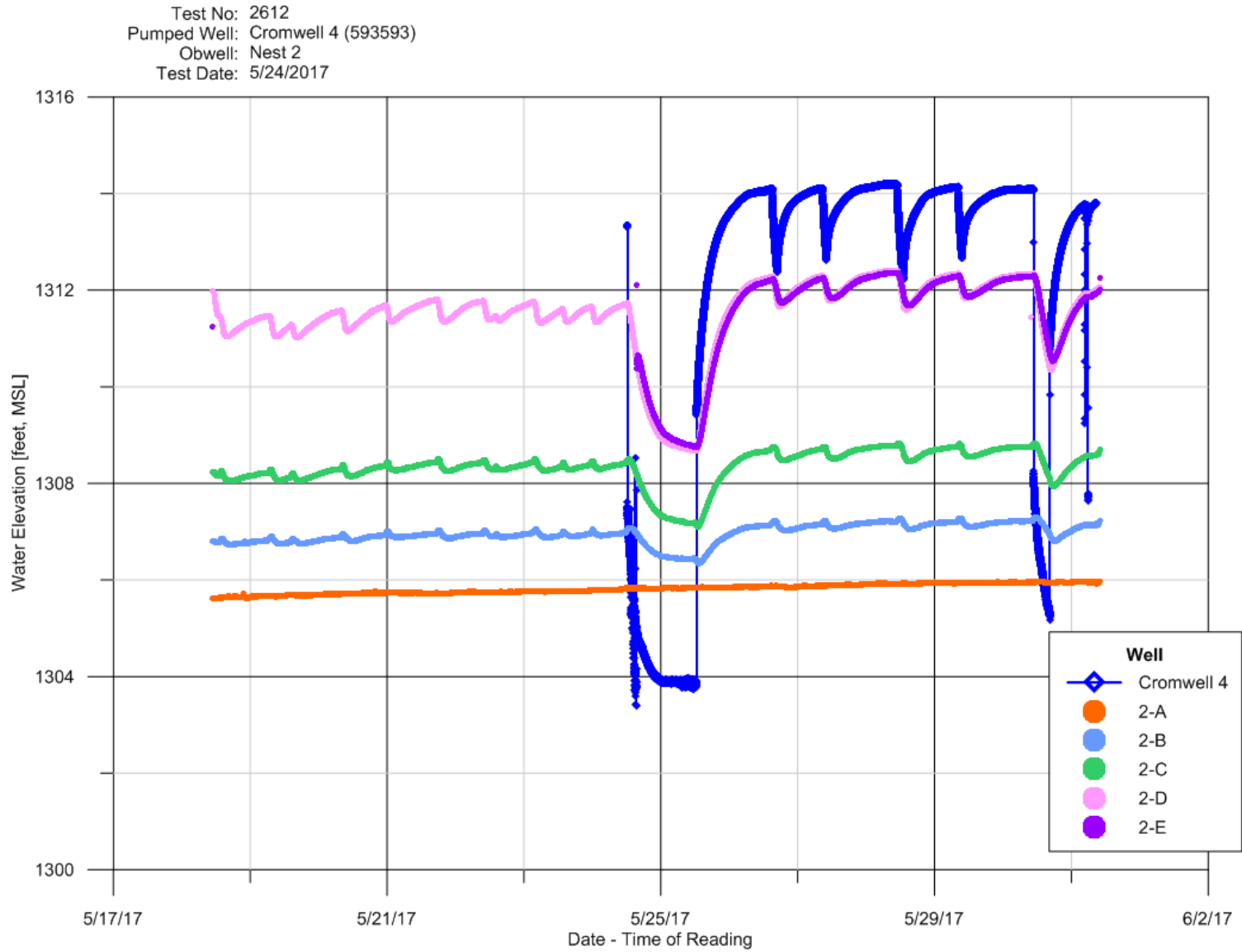


Figure 40. Time-series of Groundwater Elevation Collected at Cromwell 4 and Nest 2



TEST 2612, CROMWELL 4 (593593) MAY 24, 2017

Figure 41. Time-series of Groundwater Elevation Collected at USGS 2-A and Barometric Pressure as Difference in Water Level

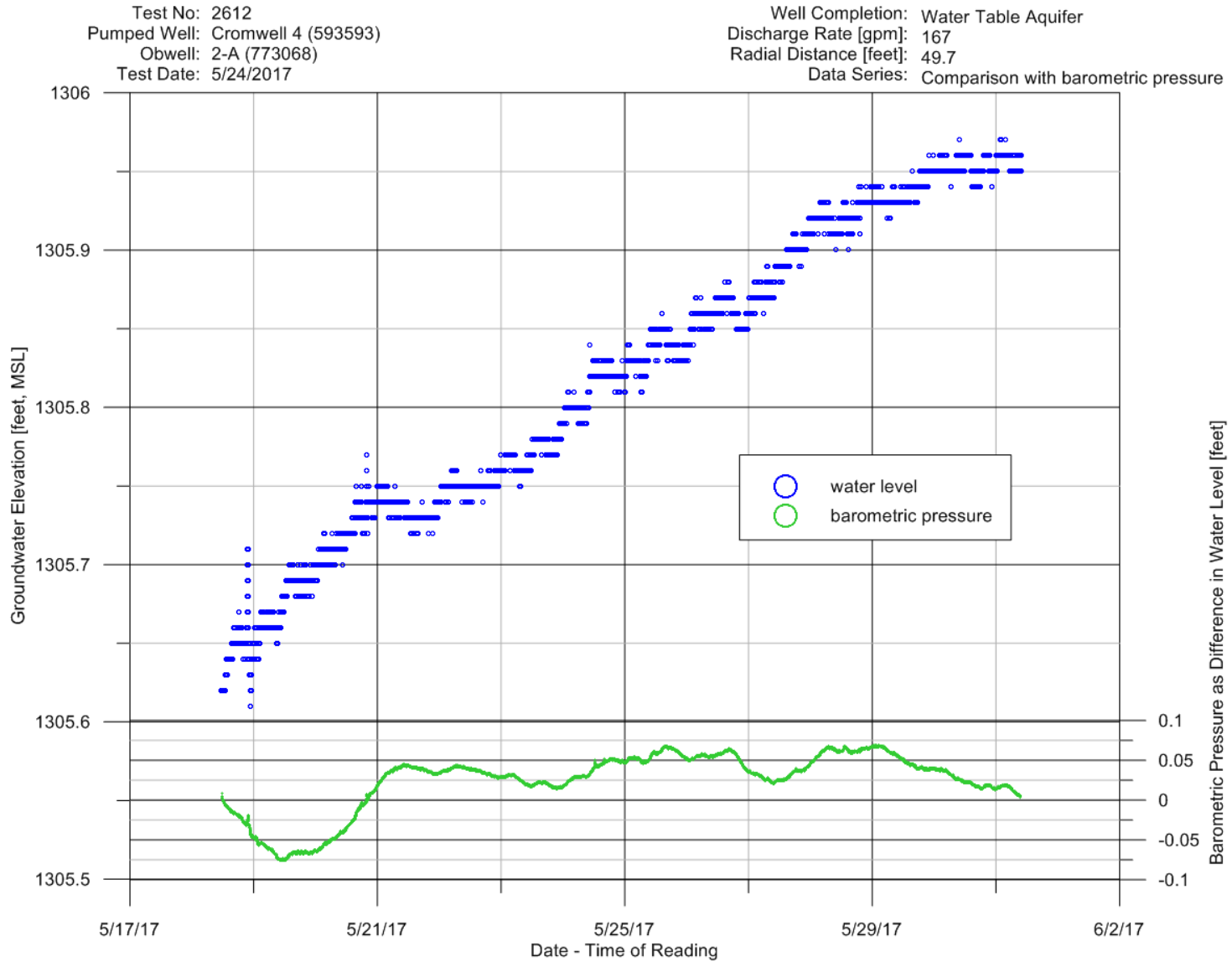
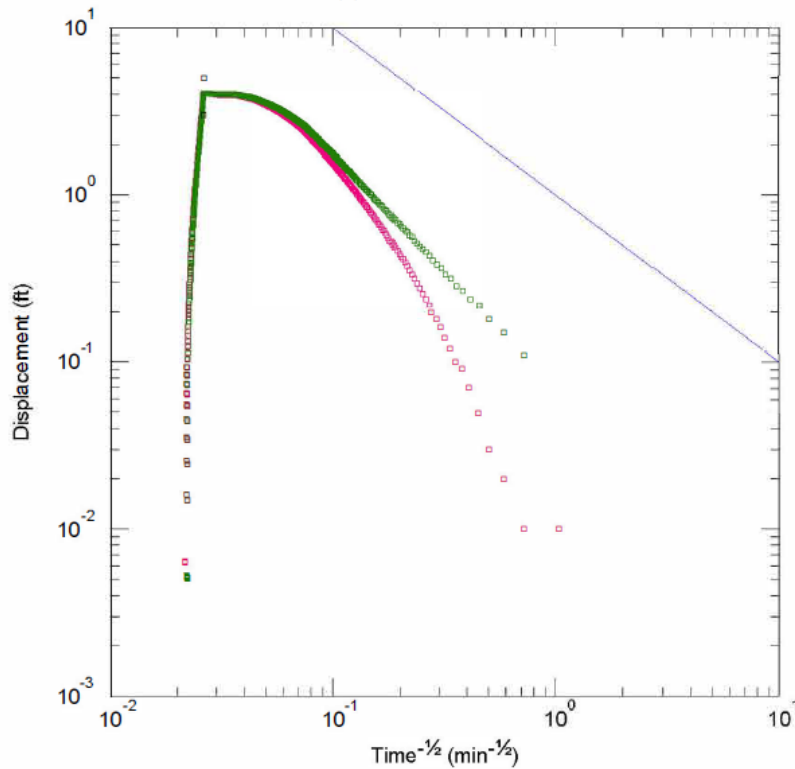


Figure 42. Aqtesolv plot of diagnostic slope for spherical flow and data from USGS 1-B and 1-C



<u>WELL TEST ANALYSIS</u>					
Data Set: O:\...\cromwell_nest-1_hantush_partial_1-Bonly_spherical.aqt					
Date: 08/18/17			Time: 16:44:40		
<u>PROJECT INFORMATION</u>					
Company: MDH					
Client: City of Cromwell					
Location: Cromwell 4					
Test Well: C-4 (593593)					
Test Date: 5/24/2017					
<u>AQUIFER DATA</u>					
Saturated Thickness: 145. ft			Anisotropy Ratio (Kz/Kr): 1.		
Aquitard Thickness (b'): 130. ft			Aquitard Thickness (b''): 20. ft		
<u>WELL DATA</u>					
Pumping Wells			Observation Wells		
Well Name	X (ft)	Y (ft)	Well Name	X (ft)	Y (ft)
Cromwell 4	0	0	1-C	139	0
			1-B	140.5	0
			1-A	142	0
			Nest 1	141	0
			Nest 2	0	50
<u>SOLUTION</u>					
Aquifer Model: Leaky			Solution Method: Hantush-Jacob		
T = 1043.9 ft ² /day			S = 0.005146		
1/B = 0.004064 ft ⁻¹			Sw = 0.		
C = 0. min ² /ft ⁵			P = 2.		
Step Test Model: Jacob-Rorabaugh			s(t) = 5.641E-19Q + 0.Q ² .		
Time (t) = 1. min Rate (Q) in cu. ft/min			W.E. = 100.% (Q from last step)		

Figure 43. Conventional log-log plot of drawdown and recovery at USGS 1-B with Walton (1960) leaky type-curve

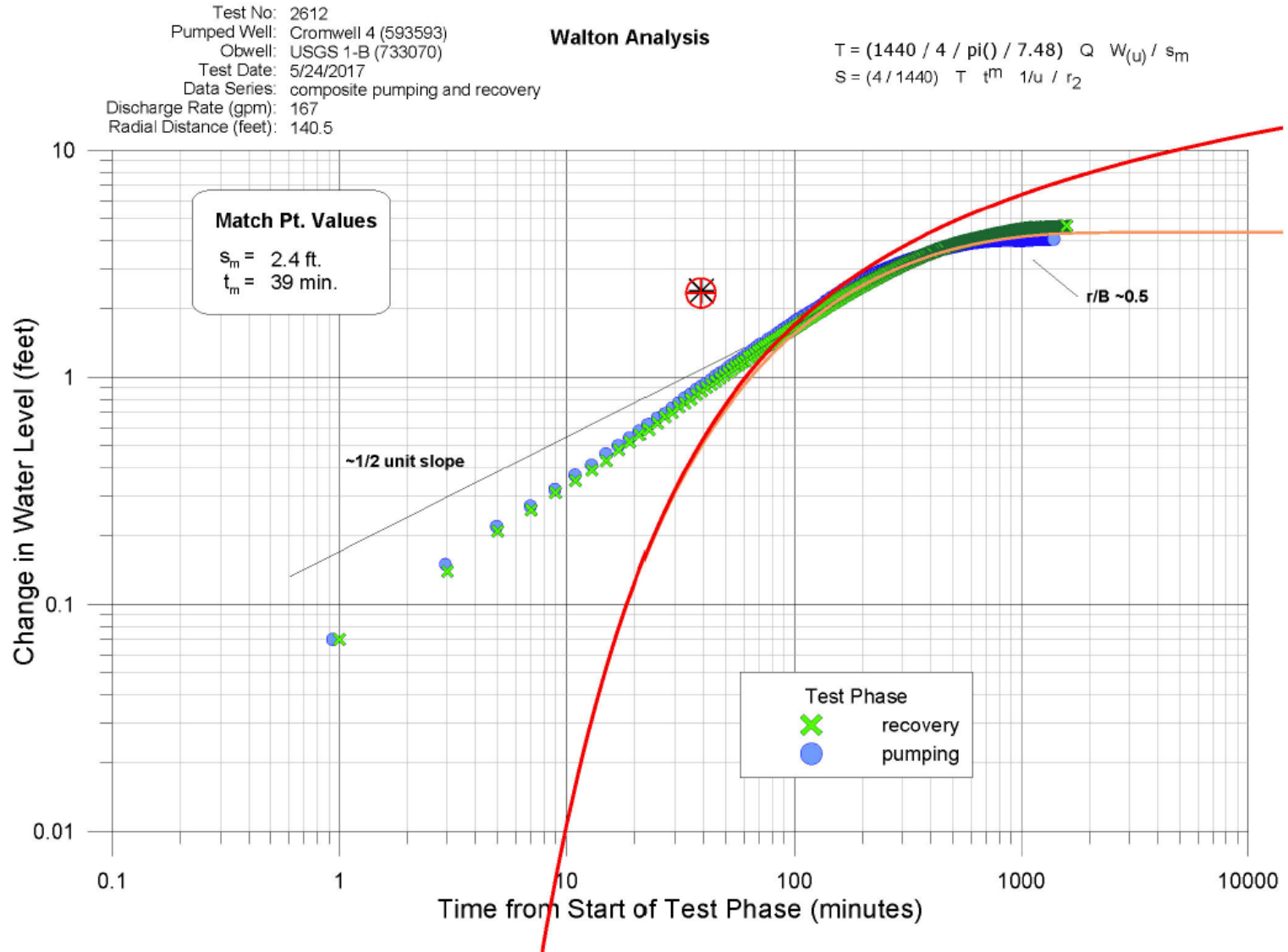


Figure 44. Conventional log-log plot of drawdown and recovery at USGS 1-C with Walton (1960) leaky type-curve

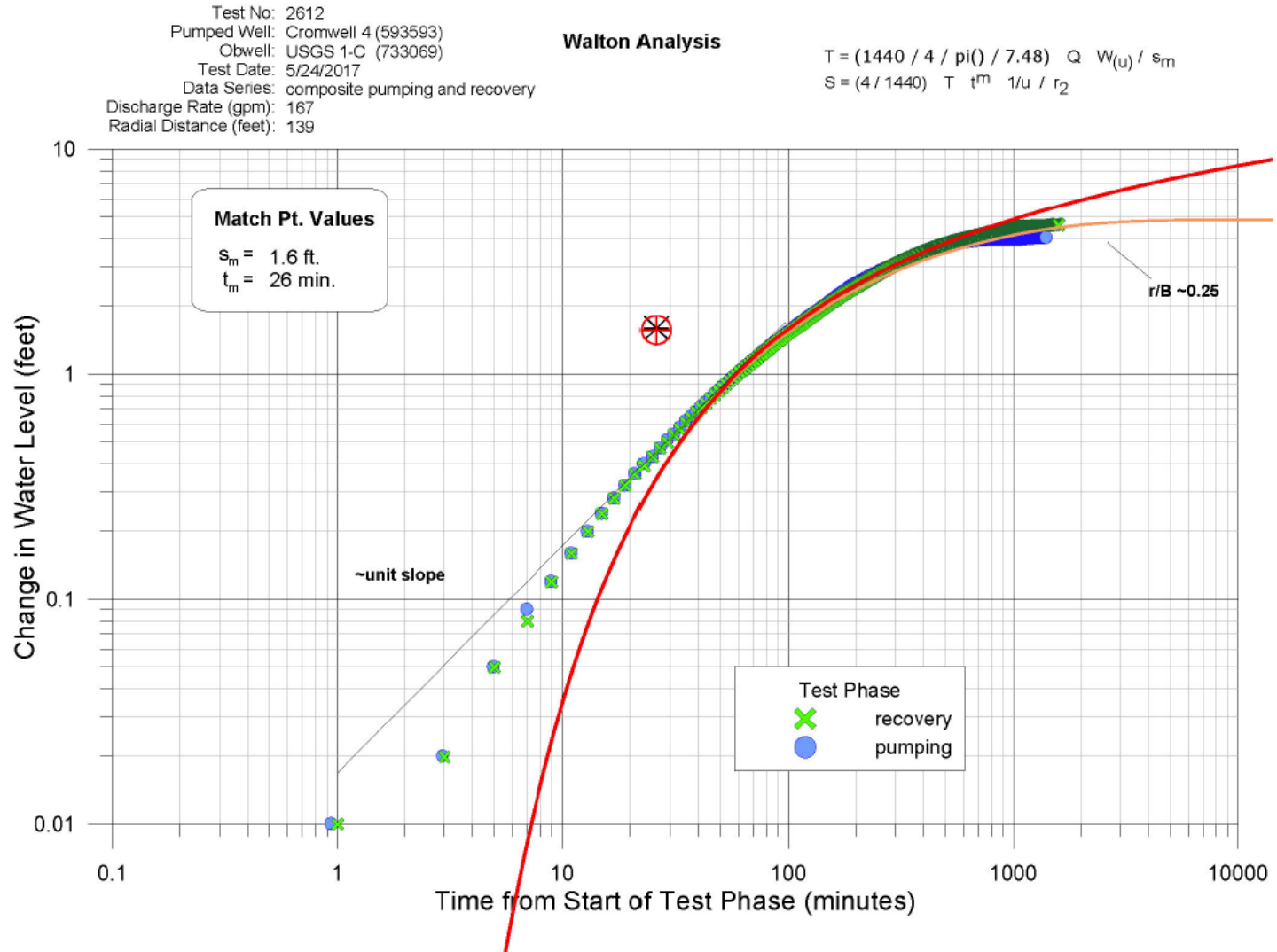


Figure 45. Well and Boring Report - Well 593593

Minnesota Unique Well Number		County		MINNESOTA DEPARTMENT OF HEALTH		Entry Date	
593593		Carlton		WELL AND BORING REPORT		03/22/2000	
		Quad Cromwell		Minnesota Statutes Chapter 1031		Update Date 03/10/2014	
		Quad ID 226B				Received Date	
Well Name	Township	Range	Dir Section	Subsection	Well Depth	Depth Completed	Date Well Completed
CROMWELL 4	49	20	W 33	CABABA	250 ft.	230 ft.	04/16/1999
Elevation	1329	Elev. Method	7.5 minute topographic map (+/- 5 feet)				
Address:							
Contact	P.O. BOX 74 CROMWELL MN 55726						
Well	CROMWELL MN 55726						
Stratigraphy Information							
Geological Material	From	To (ft.)	Color	Hardness			
CLAY	0	5	BROWN	MEDIUM			
SAND	5	40	BROWN	SOFT			
CLAY	40	80	BROWN	MEDIUM			
CLAY	80	175	GRAY	HARD			
SAND/GRAVEL	175	200	GRAY	MEDIUM			
SAND	200	240	GRAY	SOFT			
SAND/GRAVEL	240	250	GRY/BLK	MEDIUM			
Use	community supply(municipal)						Status Active
Well Hydrofractured?	Yes <input type="checkbox"/> No <input type="checkbox"/> From <input type="checkbox"/> To <input type="checkbox"/>						
Casing Type	Single casing <input type="checkbox"/> Joint <input type="checkbox"/> Welded <input type="checkbox"/>						
Drive Shoe?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/> Above/Below <input type="checkbox"/>						
Casing Diameter	Weight					Hole Diameter	
8 in. To	210 ft. 28.5 lbs./ft.					14 in. To	230 ft.
Open Hole	From	ft.	To	ft.			
Screen? <input checked="" type="checkbox"/>			Type stainless	Make JOHNSON			
Diameter	Slot/Gauge	Length	Set				
8 in.	50	22 ft.	210 ft.	230 ft.			
Static Water Level	21.2 ft. land surface Measure 04/16/1999						
Pumping Level (below land surface)	23.5 ft. 5 hrs. Pumping at 310 g.p.m.						
Wellhead Completion							
Pitless adapter manufacturer						Model	
<input checked="" type="checkbox"/> Casing Protection	<input checked="" type="checkbox"/> 12 in. above grade					<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)	
Grouting Information	Well Grouted?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Specified					
Material	Amount	From	To				
neat cement	70 Sacks	0	ft. 180	ft.			
Nearest Known Source of Contamination							
foot	Direction						Type
Well disinfected upon completion?	<input type="checkbox"/> Yes <input type="checkbox"/> No						
Pump <input type="checkbox"/> Not Installed	Date Installed	05/00/1999					
Manufacturer's name	GRUNDFOS						
Model Number	HP	Volt					
150S75-4	7.5	230					
Length of drop pipe	ft	Capacity	g.p.	Typ	Submersible		
60		150					
Abandoned	Does property have any not in use and not sealed well(s)? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No						
Variance	Was a variance granted from the MDH for this well? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No						
Miscellaneous							
First Bedrock						Aquifer	Quart. buried
Last Strat	sand +larger					Depth to Bedrock	ft
Located by	Minnesota Department of Health						
Locate Method	Digitization (Screen) - Map (1:24,000)						
System	UTM - NAD83, Zone 15, Meters	X	508617	Y	5170337		
Unique Number Verification						Input Date	08/09/2000
Angled Drill Hole							
Well Contractor							
Ranmer E.H. Well	71015					PRAUGHT, V.	
Licensee Business	Lic. or Reg. No.					Name of Driller	
Minnesota Well Index Report	593593		Printed on 05/19/2017				
							HE-01205-15

Figure 46. Well and Boring Report - Well 519761

Minnesota Unique Well Number		County		MINNESOTA DEPARTMENT OF HEALTH		Entry Date			
519761		Carlton		WELL AND BORING REPORT		03/04/1993			
		Cromwell		Minnesota Statutes Chapter 1031		Update Date 03/10/2014			
		226B				Received Date			
Well Name	Township	Range	Dir Section	Subsection	Well Depth	Depth Completed	Date Well Completed		
CROMWELL 3	49	20	W 33	CABAAB	190 ft.	190 ft.	10/21/1992		
Elevation	1325	Elev. Method	Calc from DEM (USGS 7.5 min or equiv.)						
Address:									
Contact	P.O. BOX 74 CROMWELL MN 55726								
Well	CROMWELL MN 55726								
Stratigraphy Information									
Geological Material	From	To (ft.)	Color	Hardness					
SANDY CLAY	0	12	BROWN	MEDIUM					
SAND WITH CLAY	12	30	BROWN	MEDIUM					
SAND	30	55	BROWN	SOFT					
FINE SAND	55	62	BROWN	SOFT					
FINE SAND & ROCKS	62	90	BROWN	HARD					
COARSE SAND	90	92	BROWN	SOFT					
CEMENTED SAND &	92	112	BROWN	HARD					
CEMENTED SAND &	112	132	BROWN	MEDIUM					
CEMENTED SAND &	132	172	BROWN	MED-HRD					
MIXED SAND	172	180	BROWN	SOFT					
COARSE SAND	180	190	BROWN	SOFT					
Well Hydrofractured?					Yes	<input type="checkbox"/>	No	<input type="checkbox"/>	
Casing Type					Single casing	<input checked="" type="checkbox"/>	Joint	<input type="checkbox"/>	
Drive Shoe?					Yes	<input checked="" type="checkbox"/>	No	<input type="checkbox"/>	
Casing Diameter					Weight	Hole Diameter			
8 in. To 180 ft.					28.5 lbs./ft.	10 in. To 190 ft.			
Open Hole					From	ft	To	ft	
Screen?					<input checked="" type="checkbox"/>	Type	stainless	Make	COOK
Diameter					Slot/Gauze	Length	Set		
8 in.					25	10 ft.	180 ft.	190 ft.	
Static Water Level					16 ft.	land surface	Measure	10/20/1992	
Pumping Level (below land surface)					32.1 ft.	24 hrs.	Pumping at	290 g.p.m.	
Wellhead Completion									
Pitless adapter manufacturer					Model				
<input type="checkbox"/> Casing Protection					<input checked="" type="checkbox"/> 12 in. above grade				
<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)									
Grouting Information					Well Grouted?	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No	<input type="checkbox"/> Not Specified	
Material					Amount	From	To		
bentonite					0	0 ft.	180 ft.		
Nearest Known Source of Contamination									
100 foot Southern Direction					Sepic tank/drain field Type				
Well disinfected upon completion?					<input type="checkbox"/> Yes	<input type="checkbox"/> No			
Pump					<input checked="" type="checkbox"/> Not Installed	Date Installed			
Manufacturer's name									
Model Number					HP	g	Volt		
Length of drop pipe					ft	Capacity	g.p.	Type	
Abandoned									
Does property have any not in use and not sealed well(s)?					<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No			
Variance									
Was a variance granted from the MDH for this well?					<input type="checkbox"/> Yes	<input type="checkbox"/> No			
Miscellaneous:									
First Bedrock					Aquifer	Quat. buried			
Last Strat sand-brown					Depth to Bedrock ft				
Located by					Minnesota Department of Health				
Locate Method					Digitization (Screen) - Map (1:24,000)				
System					UTM - NAD83, Zone 15, Meters	X 508644	Y 5170337		
Unique Number Verification					Information from	Input Date	10/18/1999		
Angled Drill Hole									
Well Contractor									
Peterson Well Co.					69183	PETERSEN, D.			
Licensee Business					Lic. or Reg. No.	Name of Driller			
Minnesota Well Index Report					519761	Printed on 05/19/2017			
					HE-01205-15				

Figure 47. Well and Boring Report - Well 773071

Minnesota Unique Well Number 773071		County Carlton	MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT Minnesota Statutes Chapter 1031		Entry Date 08/14/2015		
Quad Cromwell		Update Date 10/21/2015					
Quad ID 226B		Received Date					
Well Name CWO1-A	Township 49	Range 20	Dir Section W 33	Subsection CABADB	Well Depth 150 ft.	Depth Completed 147.97 ft.	Date Well Completed 07/21/2015
Elevation 1325.9	Elev. Method LIDAR 1m DEM (MNDNR)				Drill Method Non-specified Rotary	Drill Fluid Bentonite	
Address					Use environ. bore hole	Status Active	
Contact 1220 VILLA COURT DR CROMWELL MN 55726					Well Hydrofractured? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	From	To
Well 1189 VILLA VISTA CI CROMWELL MN 55726					Casing Type Single casing	Joint	
Stratigraphy Info 2960 MOODALE DR MOUNDS VIEW MN 55112					Drive Shoe? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	Above/Below	
Geological Material	From	To (ft.)	Color	Hardness	Casing Diameter	Weight	Hole Diameter
GRAVEL WITH SAND &	0	8	BRN/RED	SOFT	2 in. To	144. ft. 0.68 lbs./ft.	6.7 in. To
SILT, SAND & CLAY W/	8	11	RED/BRN	MEDIUM			150 ft.
GRAVEL & SAND WITH	11	22	GRAY	MEDIUM			
SAND & GRAVEL WITH	22	43	GRAY	MEDIUM			
SAND WITH SILT &	43	101	RED/BRN	MEDIUM			
SILT SAND CLAY	101	150	VARIED	MED-HRD			
					Open Hole	From	To
					Screen? <input checked="" type="checkbox"/>	Type slotted pipe	Make JOHNSON
					Diameter	Slot/Gauge	Length
					2 in.	10	2.8 ft.
							144.5 ft. 147.3 ft.
					Static Water Level		
					20.1 ft.	land surface	Measure 08/17/2015
					Pumping Level (below land surface)		
					ft.	6.0 hrs. Pumping at	0.79 g.p.m.
					Wellhead Completion		
					<input checked="" type="checkbox"/> Pitless adapter manufacturer	Model	
					<input checked="" type="checkbox"/> Casing Protection	<input checked="" type="checkbox"/> 12 in. above grade	
					<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)		
					Grouting Information	Well Grouted? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Specified	
					Material	Amount	From To
					bentonite	12 Sacks	2 ft. 144 ft.
					concrete	3 Sacks	ft. 2 ft.
					Nearest Known Source of Contamination		
					Well disinfected upon completion?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	Type
					Pump <input checked="" type="checkbox"/> Not Installed	Date Installed	
					Manufacturer's name		
					Model Number	HP	Volt
					Length of drop pipe	ft. Capacity	g.p. Typ
					Abandoned		
					Does property have any not in use and not sealed well(s)?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
					Variance		
					Was a variance granted from the MDH for this well?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
					Miscellaneous		
					First Bedrock	Aquifer	Quat. buried
					Last Strat	pebbly sand/silt/clay	Depth to Bedrock ft
					Located by	Minnesota Geological Survey	
					Locate Method	Digitization (Screen) - Map (1:24,000)	
					System	UTM - NAD83, Zone 15, Meters	X 508636 Y 5170295
					Unique Number Verification	Information from	Input Date
							08/14/2015
					Angled Drill Hole		
					Well Contractor		
					US Geological Survey	1548	LEIDINGER, R.
					Licensee Business	Lic. or Reg. No.	Name of Driller
Minnesota Well Index Report					773071	Printed on 05/19/2017 HE-01205-15	

Figure 48. Well and Boring Report - Well 773070

Minnesota Unique Well Number		County		MINNESOTA DEPARTMENT OF HEALTH		Entry Date	
773070		Carlton		WELL AND BORING REPORT		08/14/2015	
		Cromwell		Minnesota Statutes Chapter 1031		Update Date 10/21/2015	
		226B				Received Date	
Well Name	Township	Range	Dir Section	Subsection	Well Depth	Depth Completed	Date Well Completed
CW01-B	49	20	W 33	CABADB	230.9 ft.	230.87 ft.	07/20/2015
Elevation	1325.8	Elev. Method	LIDAR 1m DEM (MNDNR)		Drill Method	Non-specified Rotary	Drill Fluid Bentonite
Address					Use	monitor well	Status Active
Contact	1220 VILLA COURT DRIVE CROMWELL MN 55726				Well Hydrofractured?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	From To
Well	1189 VILLA VISTA CI CROMWELL MN 55726				Casing Type	Single casing	Joint
Stratigraphy Information					Drive Shoe?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	Above/Below
1189 VILLA VISTA CI CROMWELL MN 55726					Casing Diameter	Weight	Hole Diameter
Geological Material	From	To (ft.)	Color	Hardness	2 in. To	220. ft.	0.68 lbs./ft.
GRAVEL WITH SAND &	0	8	BRN/RED	SOFT			6.7 in. To 23.5 ft.
SILT, SAND & CLAY	8	11	RED/BRN	MEDIUM			
GRAVEL & SAND WITH	11	22	GRAY	MEDIUM			
SAND & GRAVEL WITH	22	43	GRAY	MEDIUM			
SAND WITH SILT AND	43	101	RED/BRN	MEDIUM			
SILT, SAND, CLAY	101	173	VARIED	MED-HRD			
SAND & GRAVEL	173	231	VARIED	MED-HRD			
Open Hole					From	ft.	To
Screen?					<input checked="" type="checkbox"/>	Type	slotted pipe
Diameter					2 in.	Slot/Gauze	Length
					20		9.6 ft.
Set					220.9 ft.		230.5 ft.
Static Water Level					16.7 ft.	land surface	Measure
							08/17/2015
Pumping Level (below land surface)					ft.	3.9 hrs.	Pumping at
							1.35 g.p.m.
Wellhead Completion					Pitless adapter manufacturer		Model
					<input checked="" type="checkbox"/>	Casing Protection	<input checked="" type="checkbox"/> 12 in. above grade
					<input type="checkbox"/>	At-grade (Environmental Wells and Borings ONLY)	
Grouting Information					Well Grouted?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Specified	
Material					Amount	From	To
bentonite					12 Sacks	2	ft. 215.7 ft.
concrete					3 Sacks		ft. 2 ft.
Nearest Known Source of Contamination					feet	Direction	Type
Well disinfected upon completion?					<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
Pump					<input checked="" type="checkbox"/> Not Installed <input type="checkbox"/> Date Installed		
Manufacturer's name							
Model Number					HP		Volt
Length of drop pipe					ft	Capacity	g.p. Typ
Abandoned					Does property have any not in use and not sealed well(s)?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
Variance					Was a variance granted from the MDH for this well?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
Miscellaneous					First Bedrock	Aquifer	Quat. buried
Last Strat					pobbly sand/silt/clay	Depth to Bedrock	ft
Located by					Minnesota Geological Survey		
Locate Method					Digitization (Screen) - Map (1:24,000)		
System					UTM - NAD83, Zone 15, Meters	X 508635	Y 5170295
Unique Number Verification					Information from	Input Date	08/14/2015
Angled Drill Hole							
Well Contractor					US Geological Survey	1548	LEININGER, R.
					Licence Business	Lic. or Reg. No.	Name of Driller
Minnesota Well Index Report				773070	Printed on 05/19/2017		
					HE-01205-15		

Figure 49. Well and Boring Report - Well 773069

Minnesota Unique Well Number		County		MINNESOTA DEPARTMENT OF HEALTH		Entry Date		
773069		Carlton		WELL AND BORING REPORT		08/14/2015		
		Quad		MINNESOTA STATUTES CHAPTER 1031		Update Date		
		226B				10/21/2015		
						Received Date		
Well Name	Township	Range	Dir	Section	Subsection	Well Depth	Depth Completed	Date Well Completed
CW01-C	49	20	W	33	CABADB	342 ft.	339.59 ft.	07/18/2015
Elevation	1325.8	Elev. Method	LIDAR 1m DEM (MNDNR)					
Address:								
Contact 1220 VILLA COURT DRIVE CROMWELL MN 55726								
Wall 1189 VILLA VISTA CI CROMWELL MN 55726								
Stratigraphy Information 2200 DAVIDSON DR MOONDALE DR MOUNDS VIEW MN 55112								
Geological Material	From	To (ft.)	Color	Hardness				
GRAVEL WITH SAND	0	8	BRN/RED	SOFT				
SILT, SAND & CLAY	8	11	RED/BRN	MEDIUM				
GRAVEL & SAND W	11	22	GRAY	MEDIUM				
SAND & GRAVEL WITH	22	43	GRAY	MEDIUM				
SILT, SAND, CLAY	43	173	RED/BRN	HARD				
SAND & GRAVEL	173	320	VARIED	MED-HRD				
CLAY WITH SLATE	320	342	BLU/GRY	HARD				
Use environ. bore hole Status: Active								
Well Hydrofractured? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> From To								
Casing Type Single casing Joint								
Drive Shoe? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> Above/Below								
Casing Diameter			Weight			Hole Diameter		
2 in. To 330 ft.			0.68 lbs./ft.			6.7 in. To 340 ft.		
Open Hole From ft. To ft.								
Screen? <input checked="" type="checkbox"/> Type slotted pipe Make ENVIRONMENTAL								
Diameter		Slot/Gauge		Length		Set		ft.
2 in.		20		9.6 ft.		329.9 ft.		339.5 ft.
Static Water Level								
16.7 ft.			land surface			Measure		08/17/2015
Pumping Level (below land surface)								
ft.			3.9 hrs.			Pumping at		1.48 g.p.m.
Wellhead Completion								
Pitless adapter manufacturer Model								
<input checked="" type="checkbox"/> Casing Protection <input checked="" type="checkbox"/> 12 in. above grade								
<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)								
Growing Information Well Grafted? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Specified								
Material		Amount		From		To		ft.
bentonite		28 Sacks		2 ft.		324 ft.		ft.
concrete		3 Sacks		ft.		2 ft.		ft.
Nearest Known Source of Contamination								
ft.		Direction		Type				
Well disinfected upon completion? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No								
Pump <input checked="" type="checkbox"/> Not Installed Date Installed								
Manufacturer's name								
Model Number			HP			Volt		
Length of drop pipe			ft			Capacity g.p.		
Type								
Abandoned								
Does property have any not in use and not sealed well(s)? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No								
Variance								
Was a variance granted from the MDH for this well? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No								
Miscellaneous								
First Bedrock						Aquifer Quart. buried		
Last Strat pobbly sand/silt/clay-gray						Depth to Bedrock ft		
Located by Minnesota Geological Survey								
Locate Method Digitization (Screen) - Map (1:24,000)								
System UTM - NAD83, Zone 15, Meters			X 508633			Y 5170295		
Unique Number Verification			Information from			Input Date 08/14/2015		
Angled Drill Hole								
Well Contractor								
US Geological Survey			1548			LEIDINGER, R.		
License Business			Lic. or Reg. No.			Name of Driller		
Minnesota Well Index Report				773069				Printed on 05/19/2017
								HE-01205-15

Figure 50. Well and Boring Report - Well 773068

Minnesota Unique Well Number 773068		County Carlton Quad Cromwell Quad ID 226B	MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT <i>Minnesota Statutes Chapter 1031</i>		Entry Date 08/14/2015 Update Date 10/20/2015 Received Date		
Well Name CWO2-A	Township 49	Range 20	Dir Section W 33	Subsection CABABA	Well Depth 174 ft.	Depth Completed 35.17 ft.	Date Well Completed 07/09/2015
Elevation 1332	Elev. Method LIDAR 1m DEM (MNDNR)				Drill Method Augur (non-specified)	Drill Fluid	
Address: Well 1189 VILLA VISTA CI CROMWELL MN 55726 C/W 2280 WOODALE DR MOUNDS VIEW MN 55112					Use environ. bore hole	Status Active	
Geology Info: CROMWELL MN 55726					Well Hydrofractured? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	From To	
Geological Material From To (ft) Color Hardness					Casing Type Single casing Joint	Drive Shoe? Yes <input type="checkbox"/> No <input type="checkbox"/> Above/Below	
COARSE SAND & SILTY SANDY CLAY 0 8 RED/BRN SOFT					Casing Diameter 1.2 in.	Weight 34.8 ft.	Hole Diameter 8.2 in.
SAND & GRAVEL 11 22 GRAY HARD					To 174 ft.		
SAND & GRAVEL 22 43 GRAY HARD					Open Hole From ft. To ft.		
CLAY W/SILT & SAND, SAND, SILTY WITH 43 120 RED/BRN HARD					Screen? <input checked="" type="checkbox"/>	Type slotted pipe	Make ENVIRONMENTAL
					Diameter 1.2 in.	Slot/Gauze 10	Length 2.7 ft.
					Set 32.5 ft.		To 35.1 ft.
					Static Water Level 28.6 ft. land surface Measure 08/17/2015		
					Pumping Level (below land surface) 2.8 hrs. Pumping at 0.17 g.p.m.		
					Wellhead Completion Piless adapter manufacturer Modal		
					<input checked="" type="checkbox"/> Casing Protection	<input checked="" type="checkbox"/> 12 in. above grade	
					<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)		
					Grouting Information Well Grouted? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Specified		
					Material	Amount	From To
					well grouted, type unknown ft. ft.		
					Nearest Known Source of Contamination foot Direction Type		
					Well disinfected upon completion? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
					Pump <input checked="" type="checkbox"/> Not Installed Date Installed		
					Manufacturer's name		
					Model Number HP Volt		
					Length of drop pipe ft Capacity g.p. Typ		
					Abandoned Does property have any not in use and not sealed well(s)? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
					Variance Was a variance granted from the MDH for this well? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
					Miscellaneous First Bedrock sand+silt-brown Aquifer Quat buried		
					Last Strat Depth to Bedrock ft		
					Located by Minnesota Geological Survey		
					Locate Method Digitization (Screen) - Map (1:24,000)		
					System UTM - NAD83, Zone 15, Meters X 508625 Y 5170347		
					Unique Number Verification Information from Input Date 08/14/2015		
					Angled Drill Hole		
					Well Contractor US Geological Survey 1548 HUCKABY, J.		
					Licensee Business Lic. or Reg. No. Name of Driller		
Minnesota Well Index Report					773068		Printed on 05/22/2017 HE-01205-15

Figure 51. Well and Boring Report - Well 773067

Minnesota Unique Well Number		County Carlton		MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT <i>Minnesota Statutes Chapter 1031</i>		Entry Date 08/14/2015	
773067		Quad Cromwell				Update Date 10/20/2015	
		Quad ID 226B				Received Date	
Well Name	Township	Range	Dir Section	Subsection	Well Depth	Depth Completed	Date Well Completed
CW02-B	49	20	W 33	CABABA	60.5 ft.	59.62 ft.	07/13/2015
Elevation	1332.2	Elev. Method	LIDAR 1m DEM (MNDNR)				
Address							
Well 1189 VILLA VISTA CI CROMWELL MN 55726							
Contact 2280 WOODALE DR CROMWELL MN 55112							
Stratigraphy Information CROMWELL MN 55726							
Geological Material	From	To (ft.)	Color	Hardness			
COARSE SAND & SAND, SILTY WITH GRAVEL & SAND, SAND WITH SILT, MED. SAND&GRVL POOR. SILTY CLAY	0	8	RED/BRN	SOFT			
	8	11	RED/BRN	MEDIUM			
	11	22	DK. GRY	MEDIUM			
	22	40	DK. GRY	MEDIUM			
	40	43	DK. GRY	HARD			
	43	61	RED/BRN	HARD			
Well Construction					Drill Method	Drill Fluid	
Use environ. bore hole					Angar (non-specified)		
Well Hydrofractured? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>					From	To	
Casing Type Single casing					Joint		
Drive Shoe? Yes <input type="checkbox"/> No <input type="checkbox"/>					Above/Below		
Casing Diameter		Weight		Hole Diameter			
1.2 in. To		56.8 ft. 0.74 lbs./ft.		8.2 in. To 60.5 ft.			
Open Hole					From	To	ft.
Screen? <input checked="" type="checkbox"/>					Type	slot pipe Make ENVIRONMENTAL	
Diameter		Slot/Gauge	Length	Set			
1.2 in.		10	2.7 ft.	57 ft.	59.6 ft.		
Static Water Level							
27.9 ft.		land surface		Measure		08/18/2015	
Pumping Level (below land surface)							
ft.		2.1 hrs. Pumping at		0.15		g.p.m.	
Wellhead Completion							
Pitless adapter manufacturer					Model		
<input checked="" type="checkbox"/> Casing Protection					<input type="checkbox"/> 12 in. above grade		
<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)							
Grouting Information					Well Grouted?	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No
					Material	Amount	From To
					bentonite	6 Sacks	2 ft. 55 ft.
					concrete	1 Sacks	ft. 2 ft.
Nearest Known Source of Contamination							
feet					Direction		Type
Well disinfected upon completion? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No							
Pump <input checked="" type="checkbox"/> Not Installed <input type="checkbox"/> Date Installed							
Manufacturer's name							
Model Number				HP	Volt		
Length of drop pipe				ft. Capacity	g.p.	Typ	
Abandoned							
Does property have any not in use and not sealed well(s)? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No							
Variance							
Was a variance granted from the MDH for this well? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No							
Miscellaneous							
First Bedrock					Aquifer	Quat. buried	
Last Strat. pebbly sand/silt/clay					Depth to Bedrock ft.		
Located by Minnesota Geological Survey							
Locate Method Digitization (Screen) - Map (1:24,000)							
System UTM - NAD83, Zone 15, Meters				X 508625	Y 5170349		
Unique Number Verification				Information from	Input Date 08/14/2015		
Angled Drill Hole							
Well Contractor							
US Geological Survey				1548	HUCKABY, J.		
Licensee Business				Lic. or Reg. No.	Name of Driller		
Minnesota Well Index Report					773067		
					Printed on 05/22/2017 HE-01205-15		

Figure 52. Well and Boring Report - Well 773066

Minnesota Unique Well Number 773066		County Carlton Quad Cromwell Quad ID 226B	MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT <i>Minnesota Statutes Chapter 1031</i>		Entry Date 08/14/2015 Update Date 10/20/2015 Received Date		
Well Name CW02-C	Township 49	Range 20	Dir Section W 33	Subsection CABAAB	Well Depth 81.57 ft.	Depth Completed 81.57 ft.	Date Well Completed 07/10/2015
Elevation 1331.9	Elev. Method LIDAR 1m DEM (MNDNR)					Drill Method Augur (non-specified)	Drill Fluid
Address					Use enviro. bore hole	Status Active	
Well 1189 VILLA VISTA CI CROMWELL MN 55726					Well Hydrofractured? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> From <input type="checkbox"/> To <input type="checkbox"/>		
Contact 2280 WOODALE DR MOUNDS VIEW MN 55112					Casing Type Single casing <input type="checkbox"/> Joint <input type="checkbox"/>		
Stratigraphy Information CROMWELL MN 55726					Drive Shoe? Yes <input type="checkbox"/> No <input type="checkbox"/> Above/Below		
Geological Material	From	To (ft.)	Color	Hardness	Casing Diameter	Weight	Hole Diameter
COARSE SAND & SAND, SILTY WITH GRAVEL & SAND, SAND WITH SILT, MED. SAND&GRVL, POOR	0	8	RED/BRN	SOFT	1.2 in. To	78.7 ft. 0.74 lbs./ft.	8.2 in. To 81.5 ft.
	8	11	RED/BRN	MEDIUM			
	11	22	DK. GRY	MEDIUM			
	22	40	DK. GRY	MEDIUM			
	40	82	DK. GRY	HARD			
Open Hole					From	ft.	To
Screen? <input checked="" type="checkbox"/>					Type slot/wire	Make ENVIRONMENTAL	
Diameter					Slot/Gauge	Length	Set
1.2 in.					10	2.7 ft.	79.9 ft. 81.5 ft.
Static Water Level					ft.	land surface	Measure 08/18/2015
Pumping Level (below land surface)					ft.	12. hrs. Pumping at	0.3 g.p.m.
Wellhead Completion					Well Grouted? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Specified		
Fitless adapter manufacturer					Amount	From	To
<input checked="" type="checkbox"/> Casing Protection <input checked="" type="checkbox"/> 12 in. above grade					6 Sacks	2	ft. 73.5 ft.
<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)					concrete	1.5 Sacks	ft. 2 ft.
Nearest Known Source of Contamination					feet	Direction	Type
Well disinfected upon completion? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No							
Pump <input checked="" type="checkbox"/> Not Installed <input type="checkbox"/> Installed					Date Installed		
Manufacturer's name					HP	Volt	
Model Number					ft	Capacity	g.p.
Length of drop pipe					Typ		
Abandoned					Does property have any not in use and not sealed well(s)? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
Variance					Was a variance granted from the MDH for this well? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
Miscellaneous					First Bedrock	Aquifer	Quant. Water
Last Strat sand+silt-gray					Depth to Bedrock	ft	
Located by Minnesota Geological Survey							
Locate Method Digitization (Screen) - Map (1:24,000)							
System UTM - NAD83, Zone 15, Meters					X	508627	Y 5170347
Unique Number Verification					Information from	Input Date	08/14/2015
Angled Drill Hole							
Well Contractor					1548	HUCKABY, J.	
US Geological Survey					Lic. or Reg. No.	Name of Driller	
Licenses Business							
Minnesota Well Index Report			773066		Printed on 05/22/2017 HE-01205-15		

Figure 53. Well and Boring Report - Well 773065

Minnesota Unique Well Number		County		MINNESOTA DEPARTMENT OF HEALTH		Entry Date		
773065		Carlton		WELL AND BORING REPORT		08/14/2015		
		Cromwell		Minnesota Statutes Chapter 1031		Update Date 10/23/2015		
		226B				Received Date		
Well Name	Township	Range	Dir Section	Subsection	Well Depth	Depth Completed	Date Well Completed	
CW02-D	49	20	W 33	CABABA	107.5 ft.	106.45 ft.	06/29/2015	
Elevation	1331.9	Elev. Method	LIDAR 1m DEM (MNDNR)					
Address:								
Well	1189 VILLA VISTA CI CROMWELL MN 55726							
Contact	2280 WOODALE DR MOUNDS VIEW MN 55112							
Stratigraphy Information								
Geological Material	From	To (ft.)	Color	Hardness				
COARSE SAND & SAND, SILTY W/CLAY	0	8	RED/BRN	SOFT				
COARSE SAND & SAND W/ SILT, MED.	8	11	RED/BRN	MEDIUM				
SAND & GRVL POOR.	11	22	DK. GRY	MEDIUM				
SAND & GRVL POOR.	22	40	DK. GRY	MEDIUM				
SAND & GRVL POOR.	40	43	DK. GRY	HARD				
SAND & GRVL POOR.	43	108	RED/BRN	HARD				
Well Hydrofractured? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> From To								
Casing Type Single casing Joint								
Drive Shoe? Yes <input type="checkbox"/> No <input type="checkbox"/> Above/Below								
Casing Diameter	Weight					Hole Diameter		
1.2 in. To	103. ft. 0.74 lbs./ft.					8.2 in. To	107. ft.	
Open Hole From ft. To ft.								
Screen? <input checked="" type="checkbox"/> Type slotted pipe Make ENVIRONMENTAL								
Diameter	Slot/Gauze	Length	Set					
1.2 in.	10	2.7 ft.	103.8 ft.	106.4 ft.				
Static Water Level								
23.4 ft.	land surface	Measure	08/18/2015					
Pumping Level (below land surface)								
ft.	1.1 hrs.	Pumping at	0.33 g.p.m.					
Wellhead Completion								
Pitless adapter manufacturer Model								
<input checked="" type="checkbox"/> Casing Protection <input type="checkbox"/> 12 in. above grade								
<input type="checkbox"/> At-grade (Environmental Wells and Borings ONLY)								
GROUTING INFORMATION Well Grouted? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Specified								
Material	Amount	From	To					
bentonite	9 Sacks	2.5 ft.	92 ft.					
concrete	2 Sacks	ft.	2.5 ft.					
Nearest Known Source of Contamination								
foot Direction Type								
Well disinfected upon completion? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No								
Pump <input checked="" type="checkbox"/> Not Installed Date Installed								
Manufacturer's name								
Model Number HP Volt								
Length of drop pipe ft Capacity g.p. Typ								
Abandoned								
Does property have any not in use and not sealed well(s)? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No								
Variance								
Was a variance granted from the MDH for this well? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No								
Miscellaneous:								
First Bedrock							Aquifer	Quat. buried
Last Strat	pobbly sand/silt/clay					Depth to Bedrock	ft	
Located by Minnesota Geological Survey								
Locate Method Digitization (Screen) - Map (1:24,000)								
System UTM - NAD83, Zone 15, Meters X 508624 Y 5170347								
Unique Number Verification Information from Input Date 08/14/2015								
Angled Drill Hole								
Well Contractor								
US Geological Survey 1548 HUCKABY, J.								
Licensee Business Lic. or Reg. No. Name of Driller								
Minnesota Well Index Report				773065		Printed on 05/22/2017 HE-01205-15		

Figure 54. Well and Boring Report - Well 773064

Minnesota Unique Well Number		County		MINNESOTA DEPARTMENT OF HEALTH		Entry Date			
773064		Carlton		WELL AND BORING REPORT		08/14/2015			
		Cromwell		Minnesota Statutes Chapter 1031		Update Date 10/23/2015			
		226B				Received Date			
Well Name	Township	Range	Dir	Section	Subsection	Well Depth	Depth Completed	Date Well Completed	
CW02-E	49	20	W	33	CABABA	129.5 ft.	128.65 ft.	07/12/2015	
Elevation	1331.9	Elev. Method	LIDAR 1m DEM (MNDNR)						
Address:									
Well 1189 VILLA VISTA CI CROMWELL MN 55726									
Contact 2280 WOODALE DR MOUNDS VIEW MN 55112									
Stratigraphy Information									
Geological Material	From	To (ft.)	Color	Hardness					
COARSE SAND &	0	8	RED/BRN	SOFT					
SAND, SILTY W/CLAY	8	11	RED/BRN	MEDIUM					
GRAVEL & SAND	11	22	DK. GRY	MEDIUM					
SAND W/SILT MED. TO	22	40	DK. GRY	MEDIUM					
SAND & GRVL POOR	40	43	DK. GRY	HARD					
SILTY CLAY	43	120	RED/BRN	HARD					
SILTY SANDY CLAY	120	130	DK. BRN	HARD					
Drill Method	Augur (non-specified)					Drill Fluid			
Use	survival bore hole					Status	Active		
Well Hydrofractured?	Yes <input type="checkbox"/>	No <input type="checkbox"/>	From	To					
Casing Type	Single casing					Joint			
Drive Shoe?	Yes <input type="checkbox"/>	No <input type="checkbox"/>	Above/Below						
Casing Diameter	Weight					Hole Diameter			
1.2 in. To	125. ft.	0.74	Ibs./ft.			8.2 in. To	129. ft.		
Open Hole	From	ft.	To	ft.					
Screen?	<input checked="" type="checkbox"/>	Type	slot pipe		Make	ENVIRONMENTAL			
Diameter	Slot/Gauze	Length	Set						
1.2 in.	10	2.7	ft.	126	ft.	128.6 ft.			
Static Water Level									
23.9	ft.	land surface			Measure	08/18/2015			
Pumping Level (below land surface)									
	ft.	3.9	hrs.	Pumping at	0.4	g.p.m.			
Wellhead Completion									
Pitless adapter manufacturer						Model			
<input checked="" type="checkbox"/>	Casing Protection					<input type="checkbox"/>	12 in. above grade		
<input type="checkbox"/>	At-grade (Environmental Wells and Borings ONLY)								
Grouting Information									
Well Grouted?	<input checked="" type="checkbox"/>	Yes	<input type="checkbox"/>	No	<input type="checkbox"/>	Not Specified			
Material	Amount	From	To						
bentonite	8	Sacks	2	ft.	24.1 ft.				
concrete	2	Sacks		ft.	2 ft.				
Nearest Known Source of Contamination									
foot	Direction					Type			
Well disinfected upon completion?	<input type="checkbox"/>	Yes	<input checked="" type="checkbox"/>	No					
Pump	<input checked="" type="checkbox"/>	Not Installed		Date Installed					
Manufacturer's name						HP	Volt		
Model Number						Capacity	Typ		
Length of drop pipe	ft								
Abandoned									
Does property have any not in use and not sealed well(s)?	<input type="checkbox"/>	Yes	<input checked="" type="checkbox"/>	No					
Variance									
Was a variance granted from the MDH for this well?	<input type="checkbox"/>	Yes	<input checked="" type="checkbox"/>	No					
Miscellaneous:									
First Bedrock						Aquifer	Quat. buried		
Last Strat	pbbly sand/silt/clay-					Depth to Bedrock	ft		
Located by	Minnesota Geological Survey								
Locate Method	Digitization (Screen) - Map (1:24,000)								
System	UTM - NAD83, Zone 15, Meters		X	508624	Y	5170349			
Unique Number Verification	Information from			Input Date	08/14/2015				
Angled Drill Hole									
Well Contractor									
US Geological Survey			1548	HUCKABY, J.					
License Business			Lic. or Reg. No.	Name of Driller					
Minnesota Well Index Report				773064		Printed on 05/23/2017 HE-01205-15			